

CAP-X



Using a Small Solar Cell for Harvesting and a Supercapacitor for Power Management in a Wireless Sensor

9th June 2010

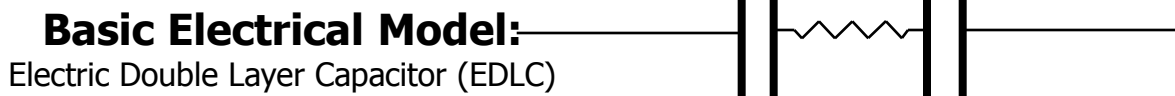
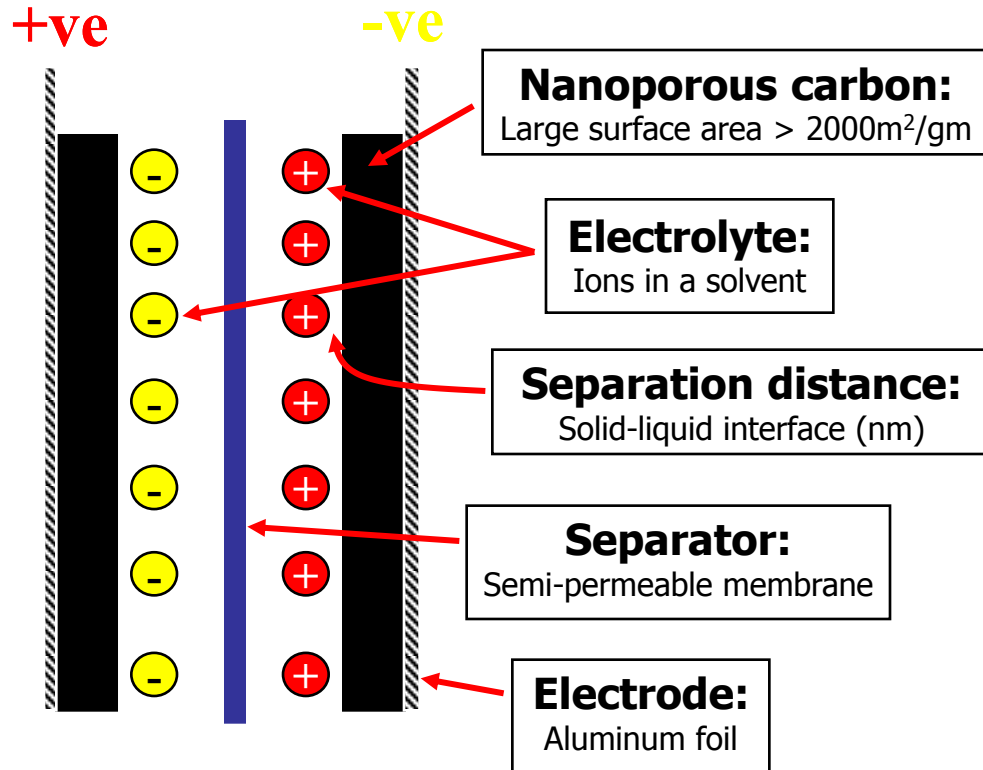
- Supercapacitor Properties
 - What's inside
 - Power buffer
 - Leakage current
 - Charge current
 - Ageing
- Solar cell characteristics
- Circuits to charge supercpacitors from solar cells
- Sizing your supercapacitor

A supercapacitor is an energy storage device which utilizes high surface area carbon to deliver much higher energy density than conventional capacitors

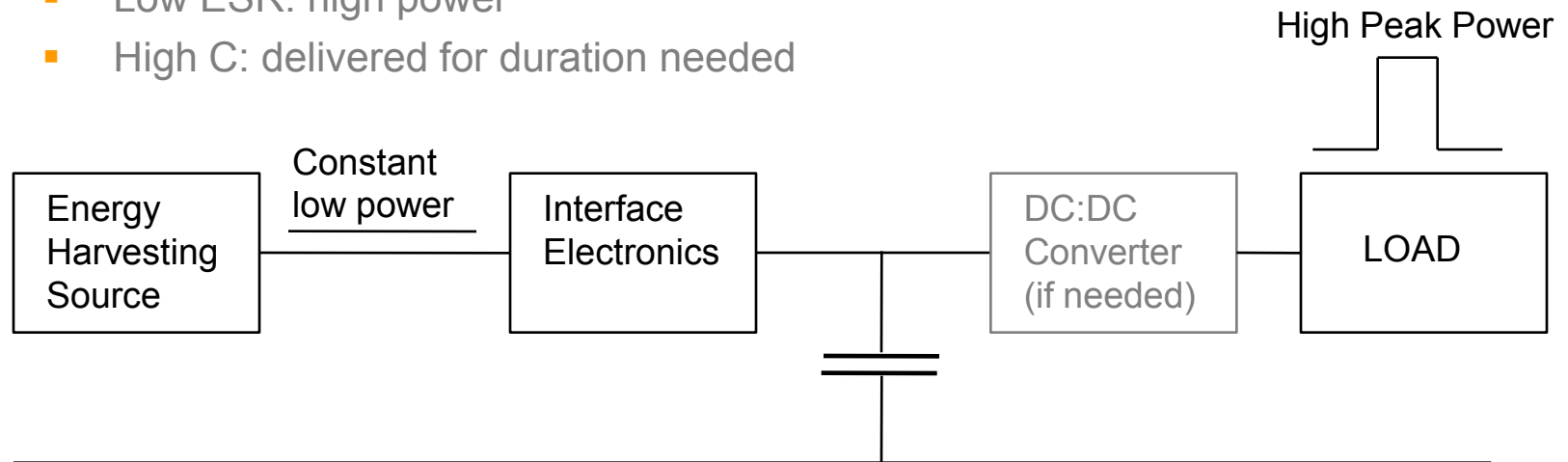
Basic Theory:
 Capacitance is proportional to the charge storage area, divided by the charge separation distance ($C \propto A / d$)

As area (A) \uparrow , and charge distance (d) \downarrow capacitance (C) $\uparrow\uparrow\uparrow$

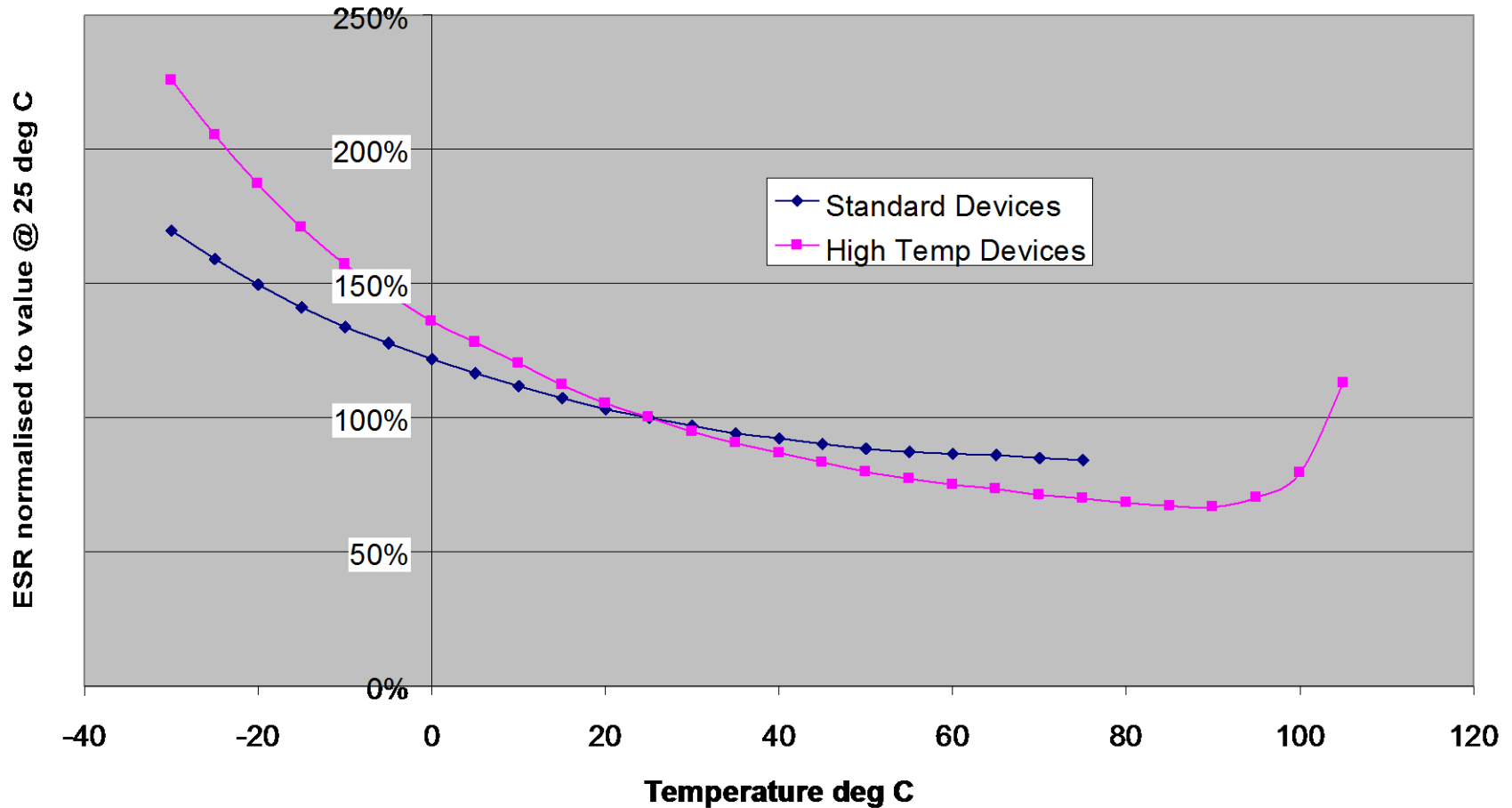
No dielectric, working voltage determined by electrolyte



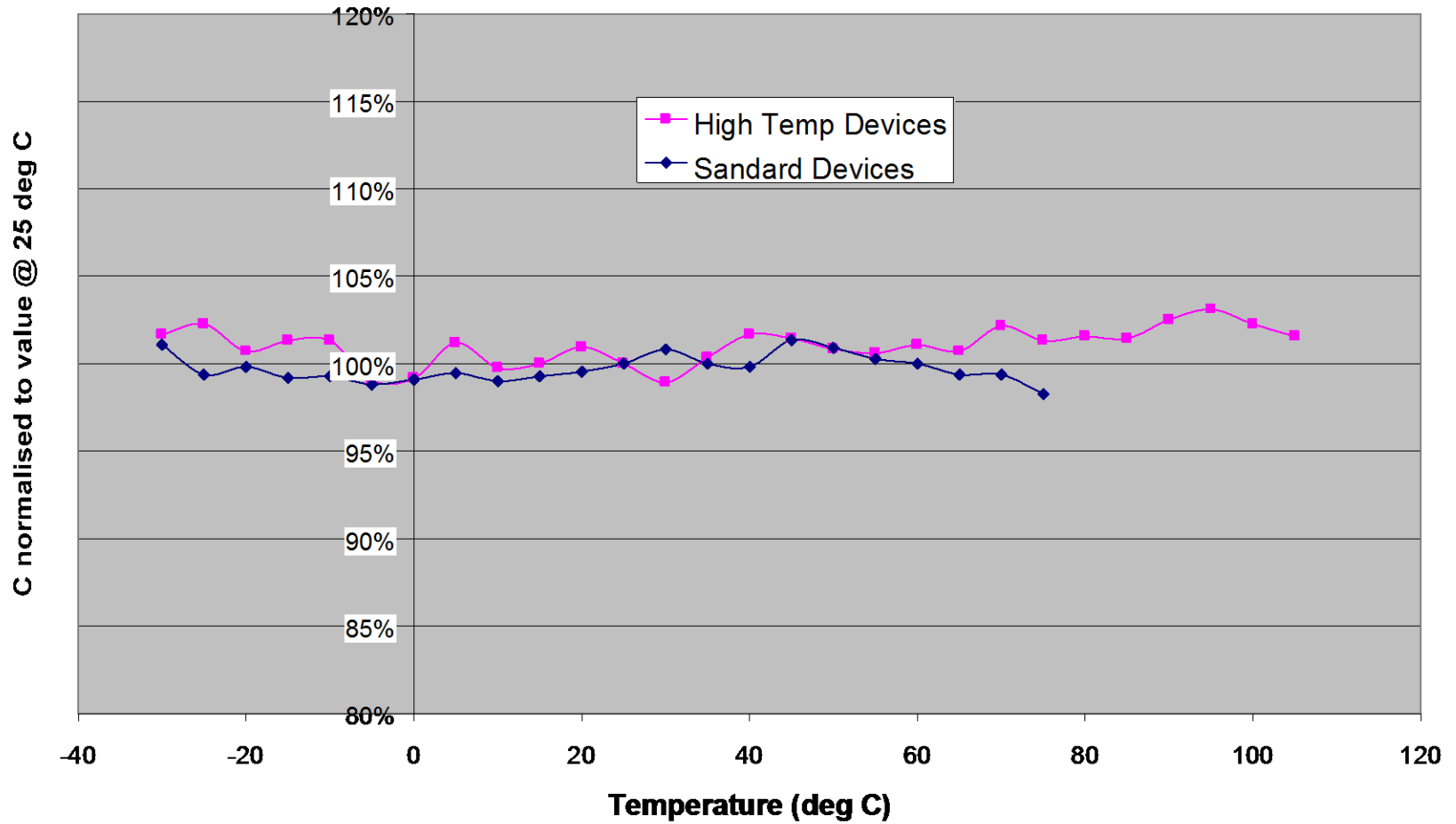
- A supercapacitor buffers the load from the source. Source provides low average power, supercapacitor provides peak power to the load.
- Average load power < Average source power
- Source sees low power load
- Load sees low impedance source that delivers high peak power for duration needed
 - Low ESR: high power
 - High C: delivered for duration needed

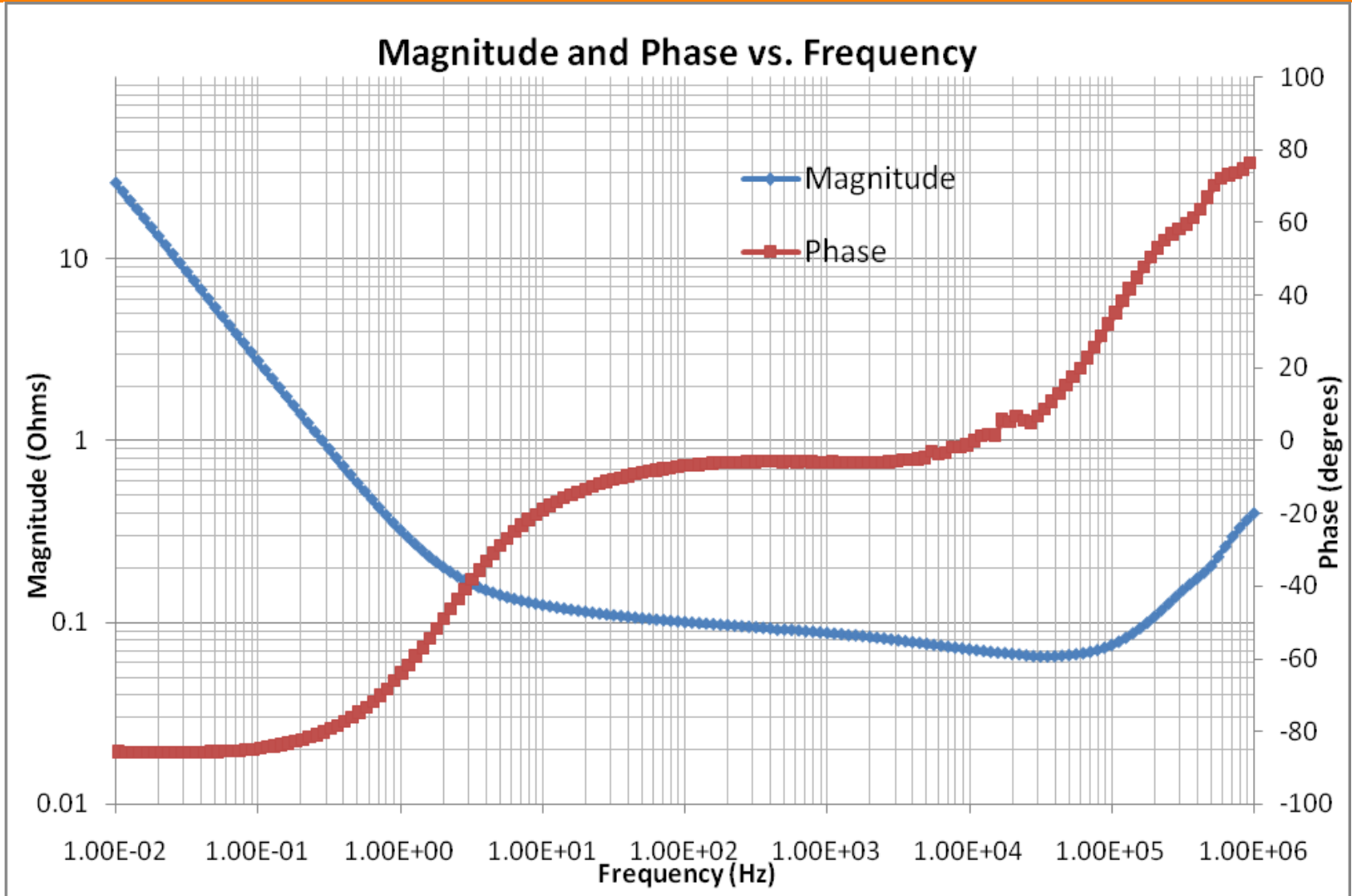


Normalised ESR vs Temp

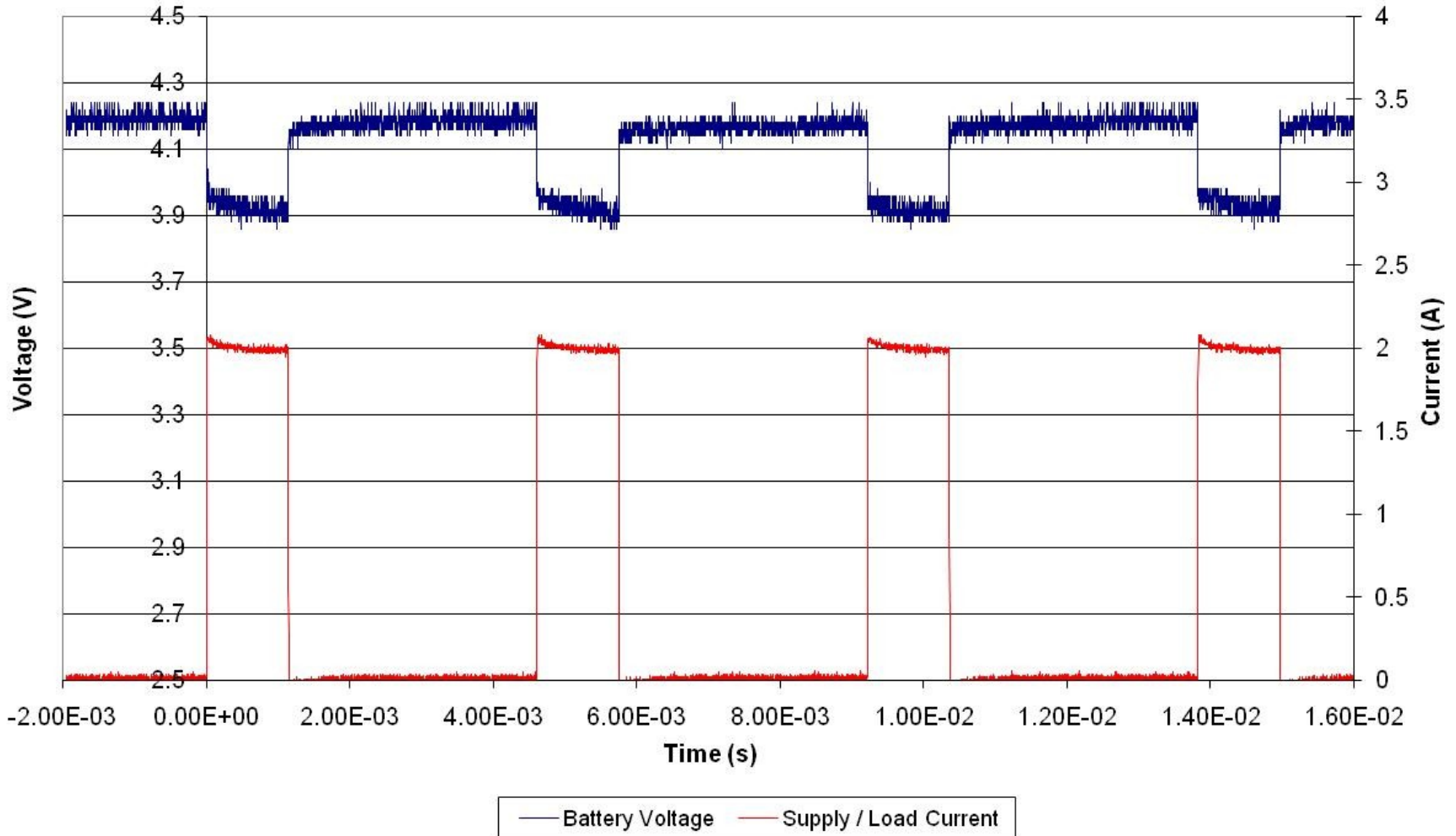


Normalised C vs Temp

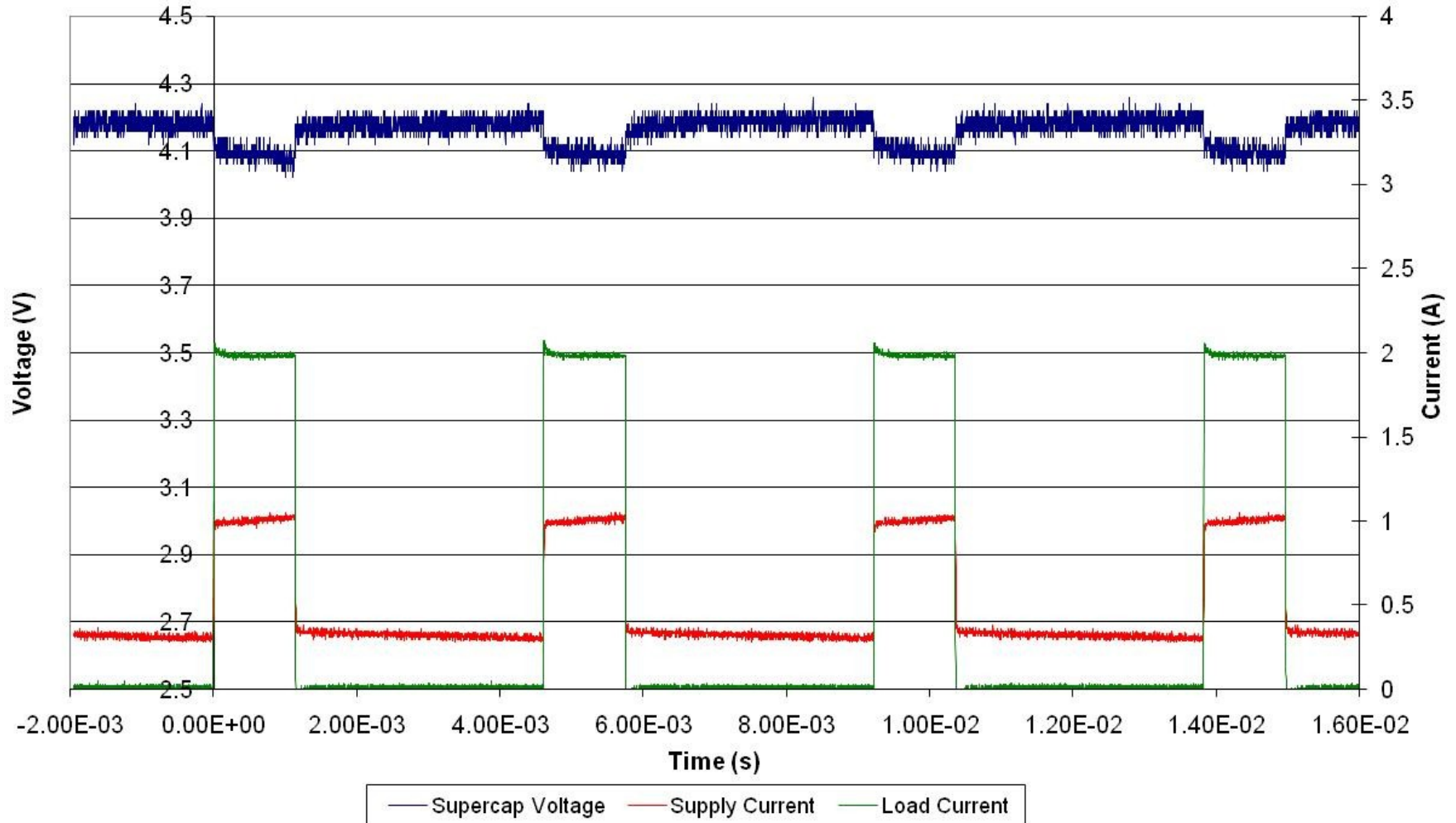


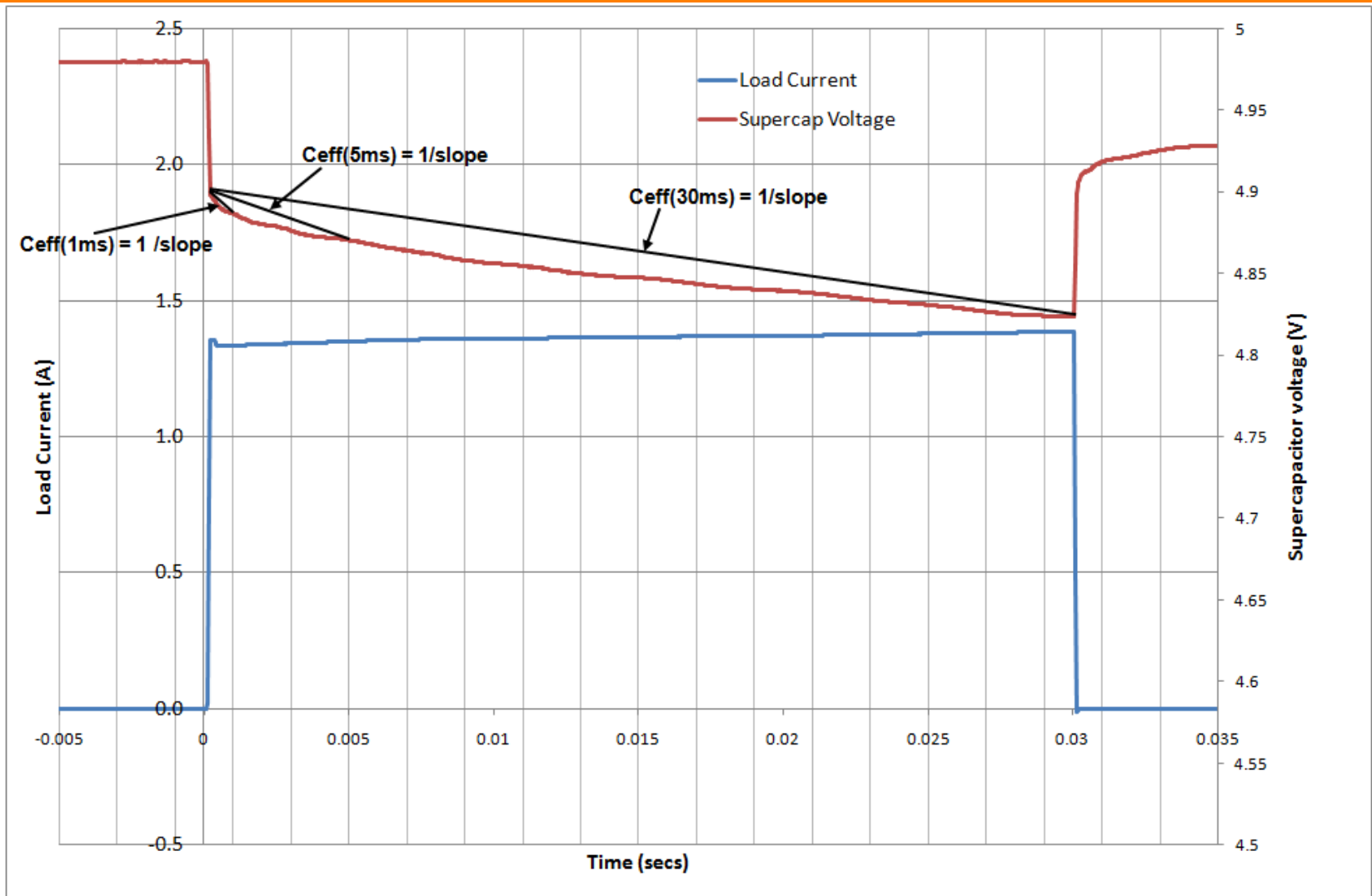


Case 1 - Battery Only

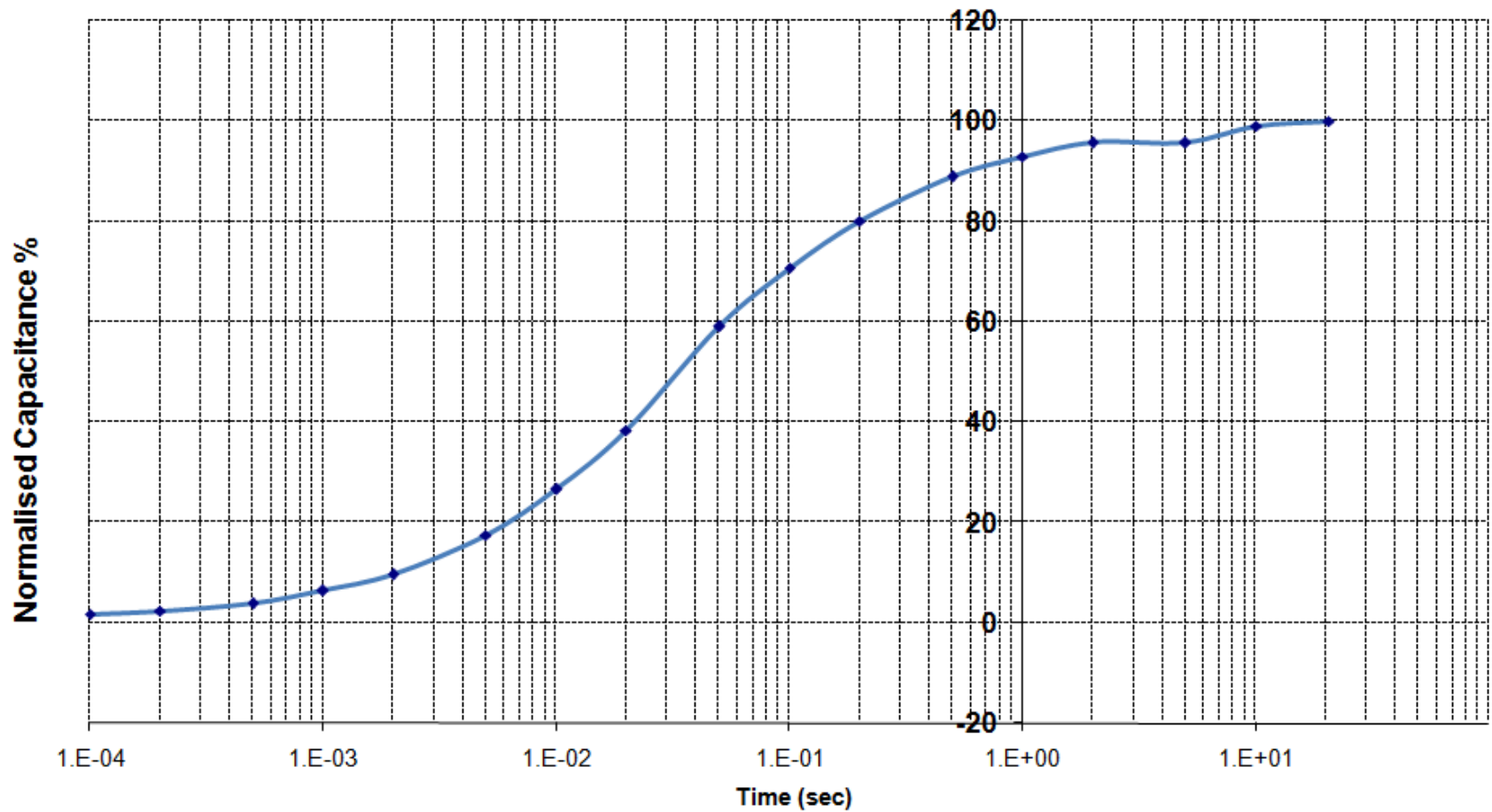


Case 2 - Nokia BL6C Battery + CAP-XX Supercapacitor





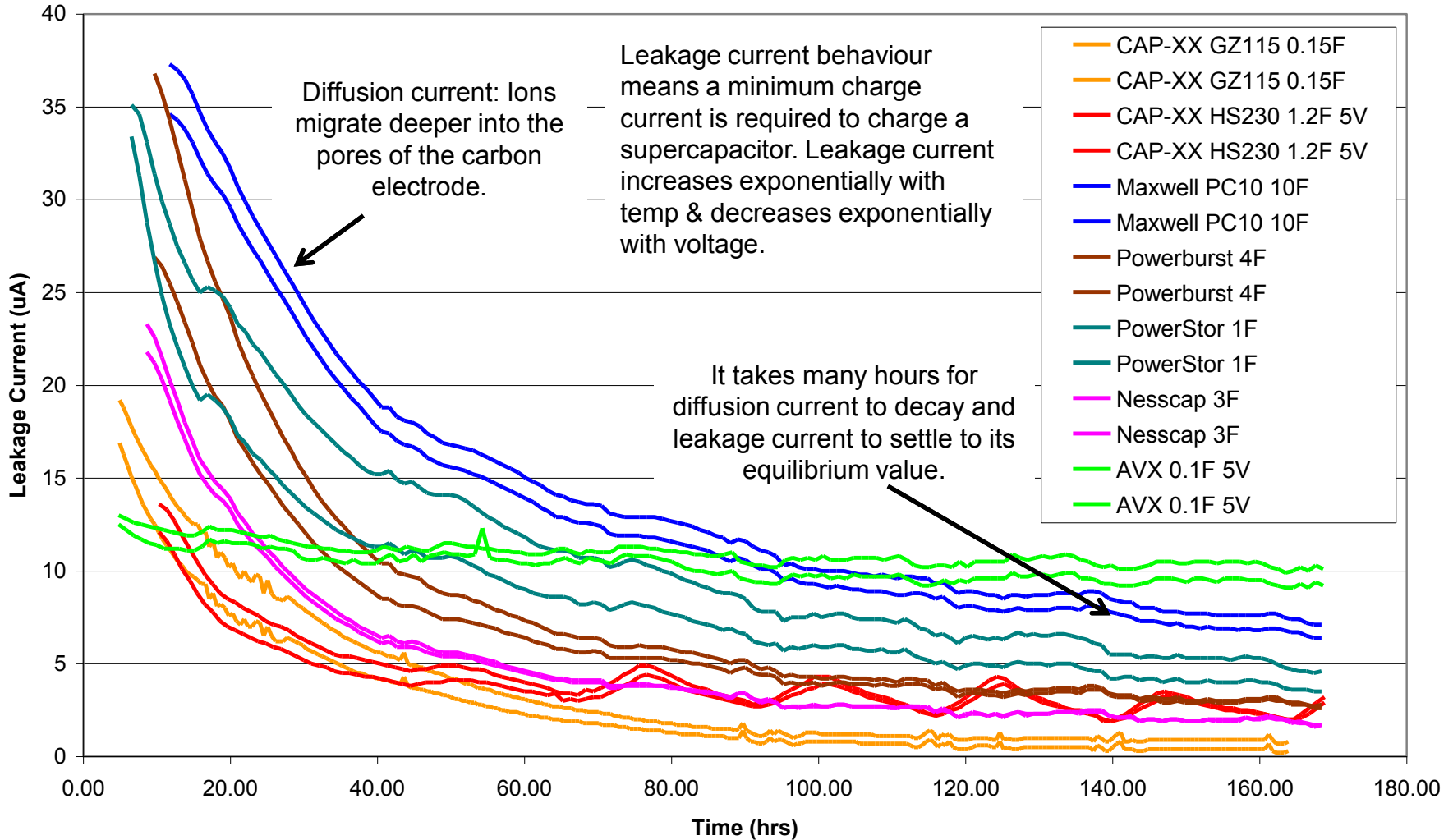
Normalised Capacitance vs Time @ 23C, CAP-XX HS206



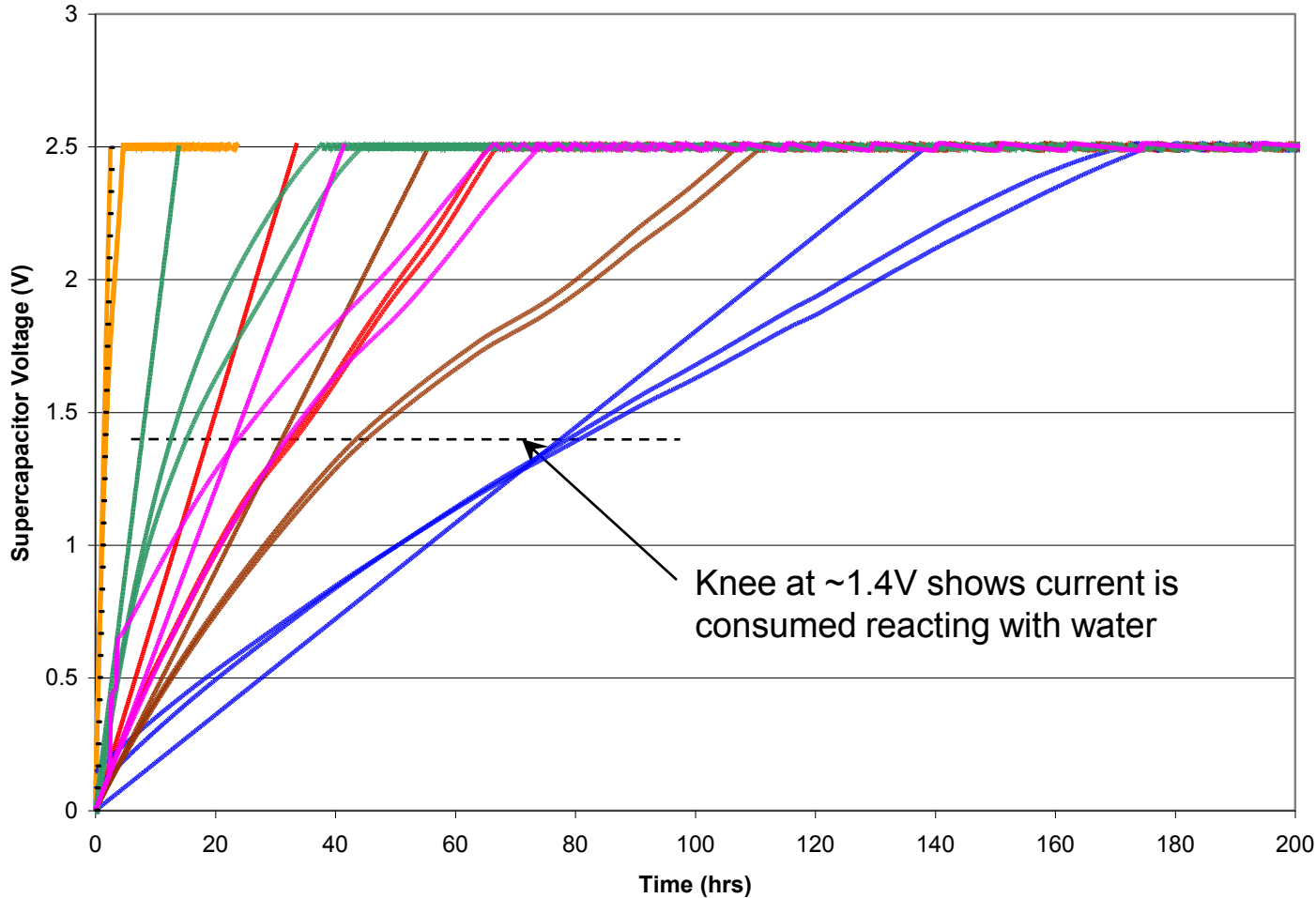
CAP-XX Required C reduces faster than Ceff

- HS206, DC Capacitance = 600mF
- $\Delta V = I \cdot \Delta t / C_{\text{eff}}$
- 2A for 1ms
 - $C_{\text{eff}} = 6.5\% \text{ of } 600\text{mF} = 39\text{mF}$
 - $\Delta V = 2\text{A} \times 1\text{ms} / 39\text{mF} = 51\text{mV}$
- 2A for 10ms
 - $C_{\text{eff}} = 26\% \text{ of } 600\text{mF} = 156\text{mF}$
 - $\Delta V = 2\text{A} \times 10\text{ms} / 156\text{mF} = 128\text{mV}$
- 2A for 100ms
 - $C_{\text{eff}} = 70\% \text{ of } 600\text{mF} = 420\text{mF}$
 - $\Delta V = 2\text{A} \times 100\text{ms} / 420\text{mF} = 476\text{mV}$

Leakage Current



Charging at 50uA



- CAP-XX HZ102 0.18F
- CAP-XX HZ102 0.18F
- Theoretical HZ102
- CAP-XX HS130 2.4F
- CAP-XX HS130 2.4F
- CAP-XX HS130 Theoretical
- Maxwell PC10 10F
- Maxwell PC10 10F
- Maxwell PC10 Theoretical
- Powerburst 4F
- Powerburst 4F
- Powerburst 4F Theoretical
- PowerStor 1F
- PowerStor 1F
- PowerStor 1F Theoretical
- Nesscap 3F
- Nesscap 3F
- Nesscap 3F Theoretical

Long Term HS108 Supercapacitor Self Discharge

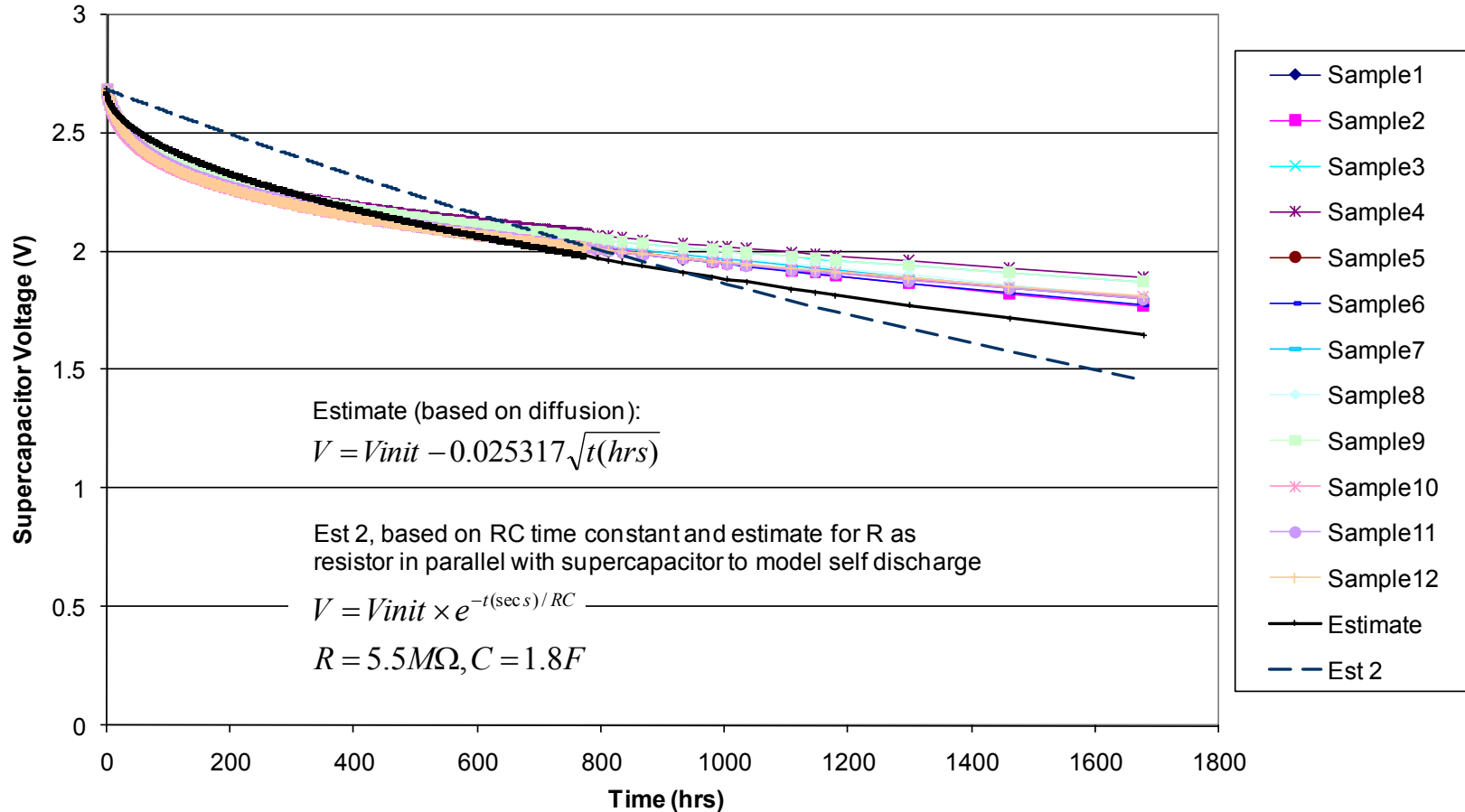
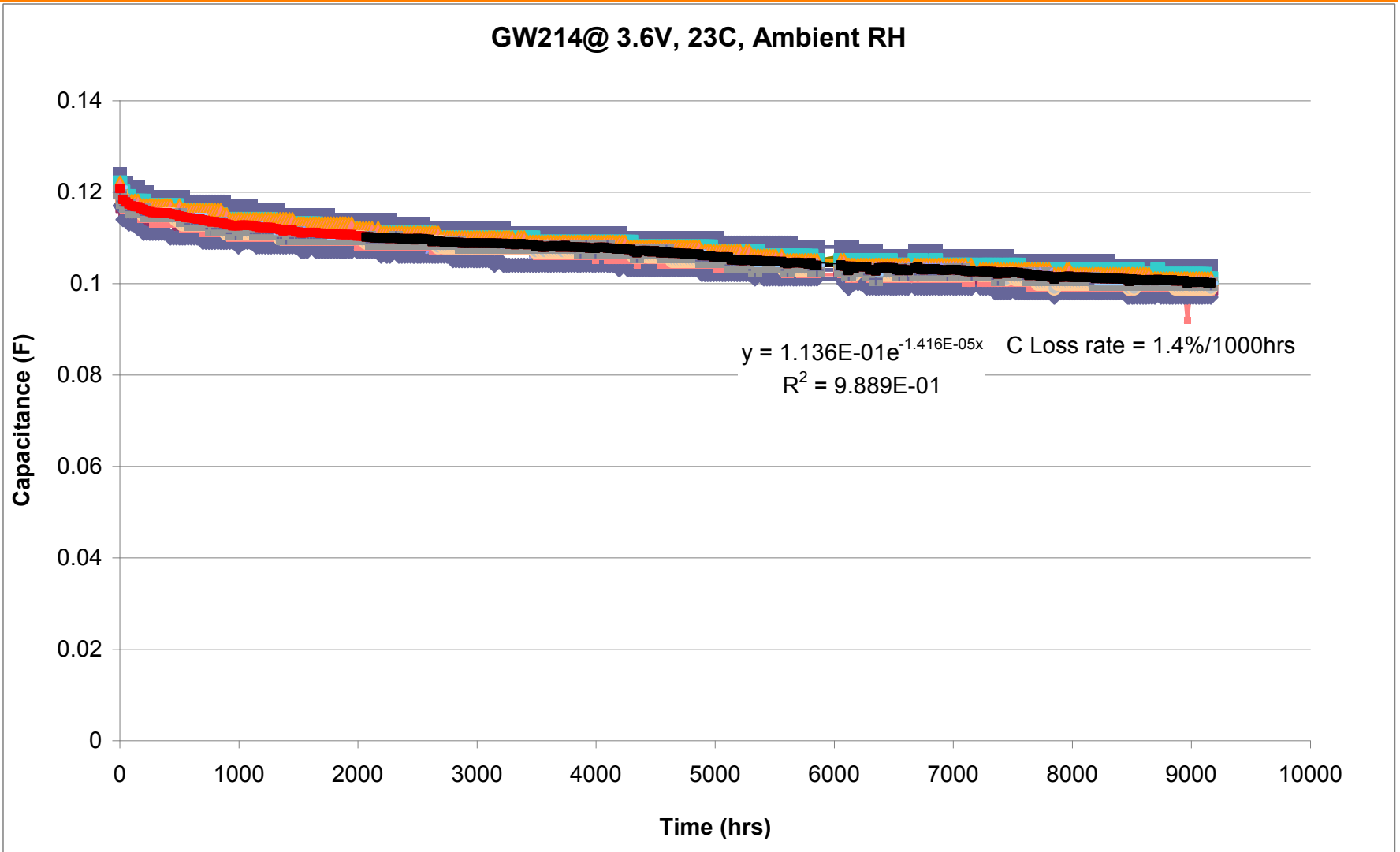
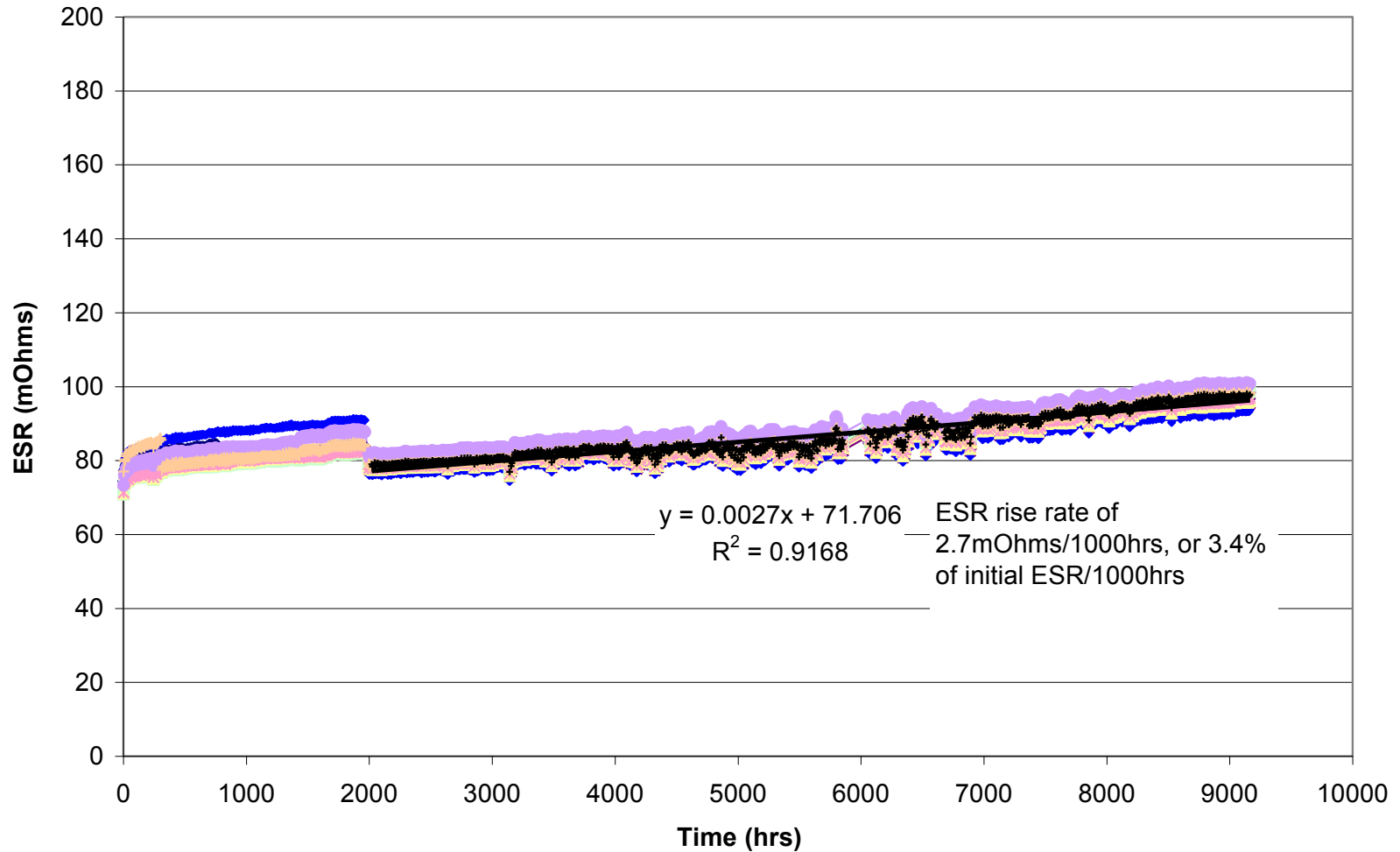


Figure 12: Supercapacitor self discharge characteristic

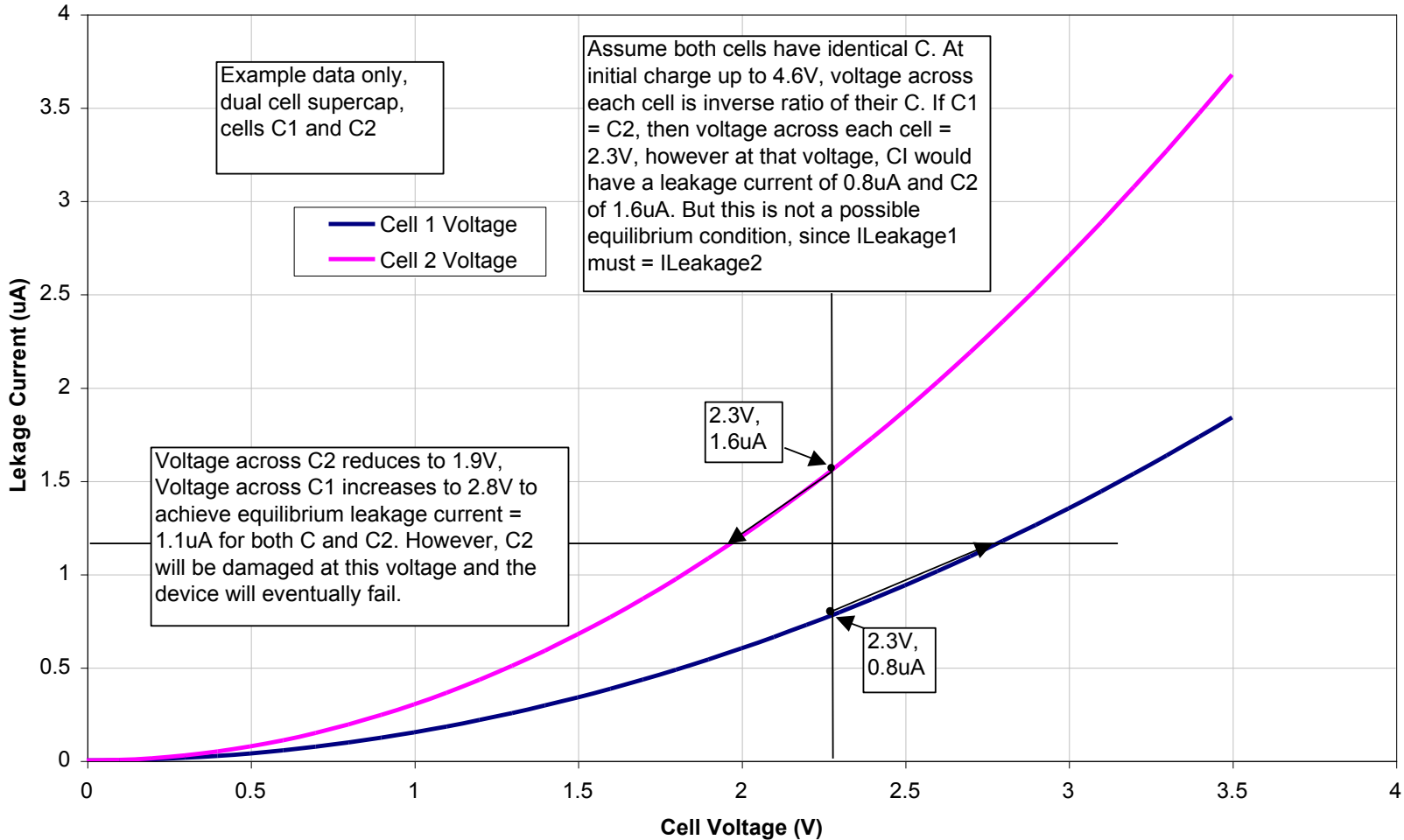
- Supercapacitors use physical not electrochemical charge storage
- Ageing is a function of time at temperature and voltage, not no. of cycles
- Determine expected ageing from operating profiles (voltage and temp combination) and their duty cycle
- Size supercapacitor so you have required C & ESR at end of life after allowing for ageing

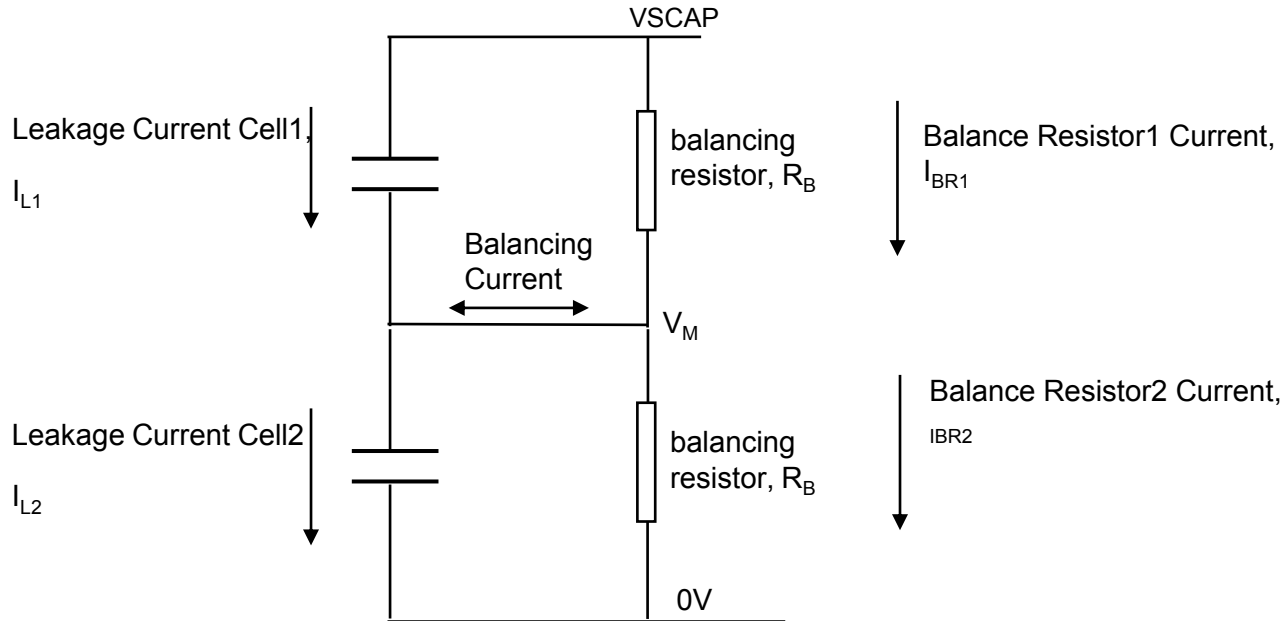


GW214 ESR @ 3.6V, 23C, Ambient RH



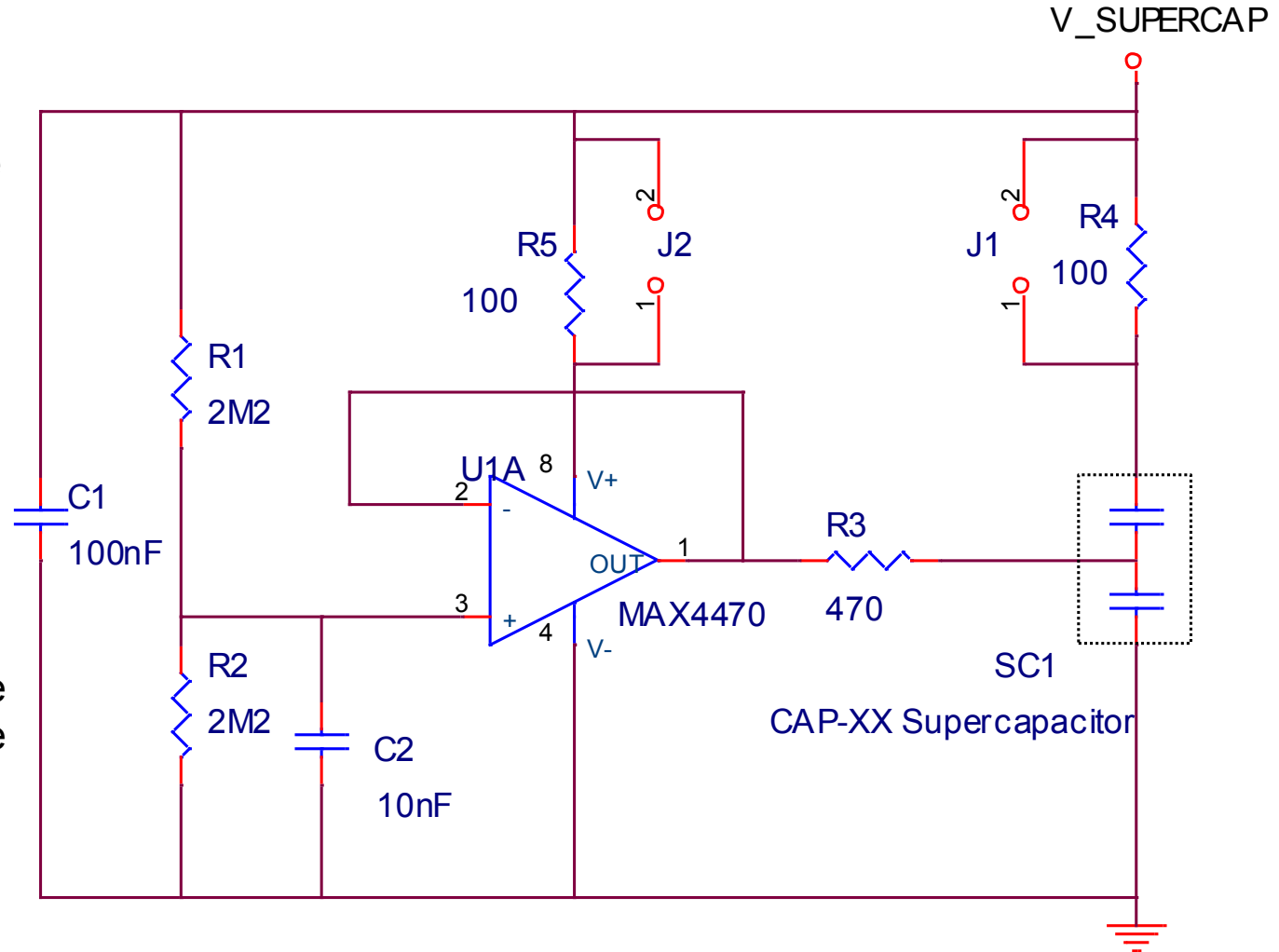
Leakage Current

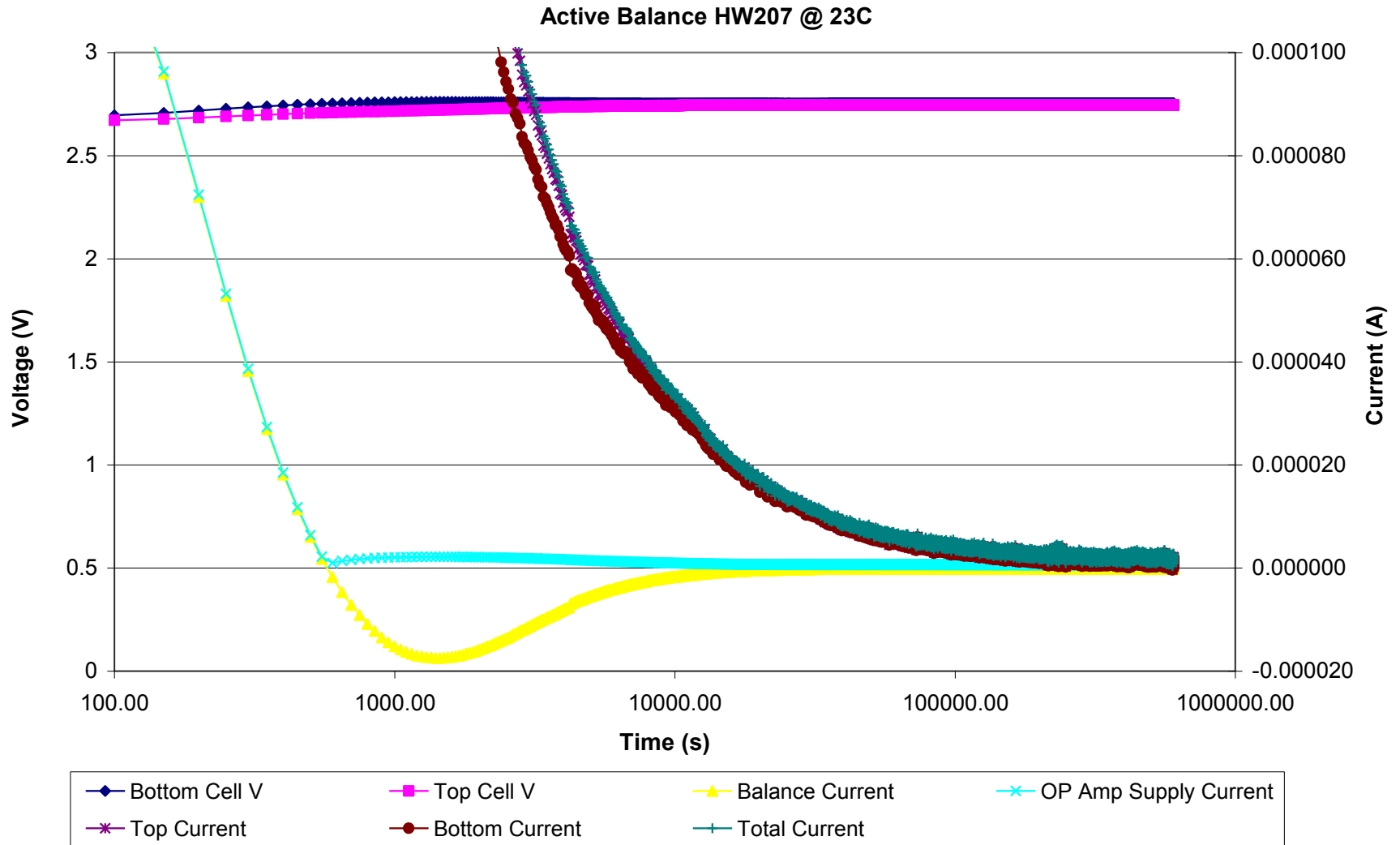


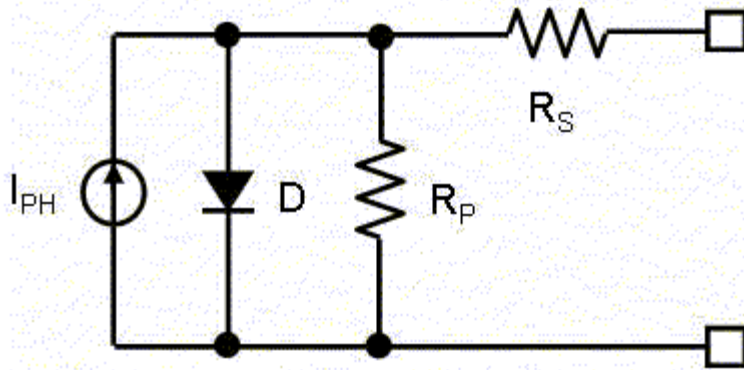


- The purpose of this circuit is to maintain V_M close to $V_{SCAP}/2$.
- $V_M = R_B \times I_{BR2} = R_B \times (I_{BR1} - \text{Balancing Current})$.
- For this circuit to work, Balancing Current must be $\ll I_{BR1}, I_{BR2}$.
- V_M must be prevented from going $\gg V_{SCAP}/2$ or $\ll V_{SCAP}$ for any significant length of time.
- SIMPLE but HIGH CURRENT SOLUTION ($\sim 100\mu A$)

- 2 capacitor cells in series need voltage balancing, otherwise slight differences in leakage current may result in voltage imbalance and one cell going over voltage.
- Low current rail-rail op amp, $< 1\mu\text{A}$
- Can source or sink current, 11mA
- Supplies or sinks the difference in leakage current between the 2 cells to maintain balance.







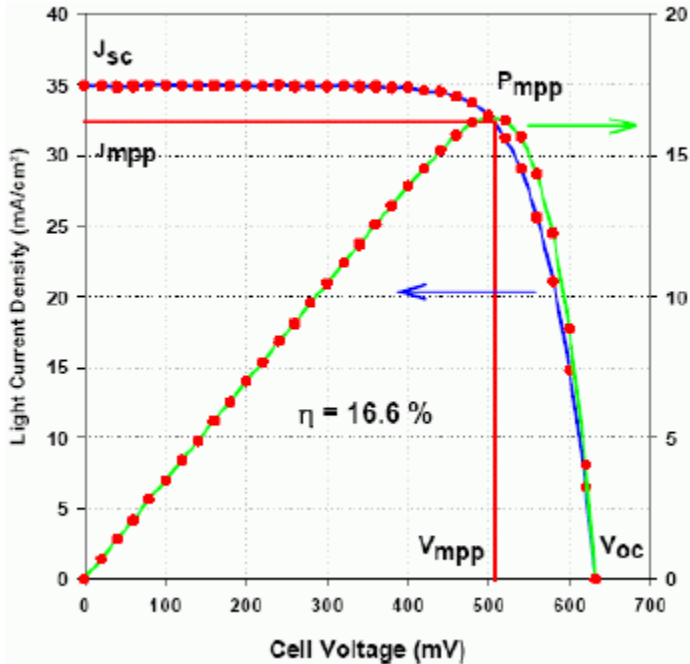
Simplified Circuit Model of a Solar Cell

XOB17, 22mm x 7mm x 1.6mm
used for measurements in
following slides



- I_{PH} generates current \propto light falling on the cell
 - If no load connected all the current flows through the diode whose forward voltage = V_{OC} .
 - R_P represents leakage current
 - R_S represents connection losses, usually not significant
-
- Will deliver current into a short circuit (discharged supercapacitor)
 - Will discharge the load if light level drops

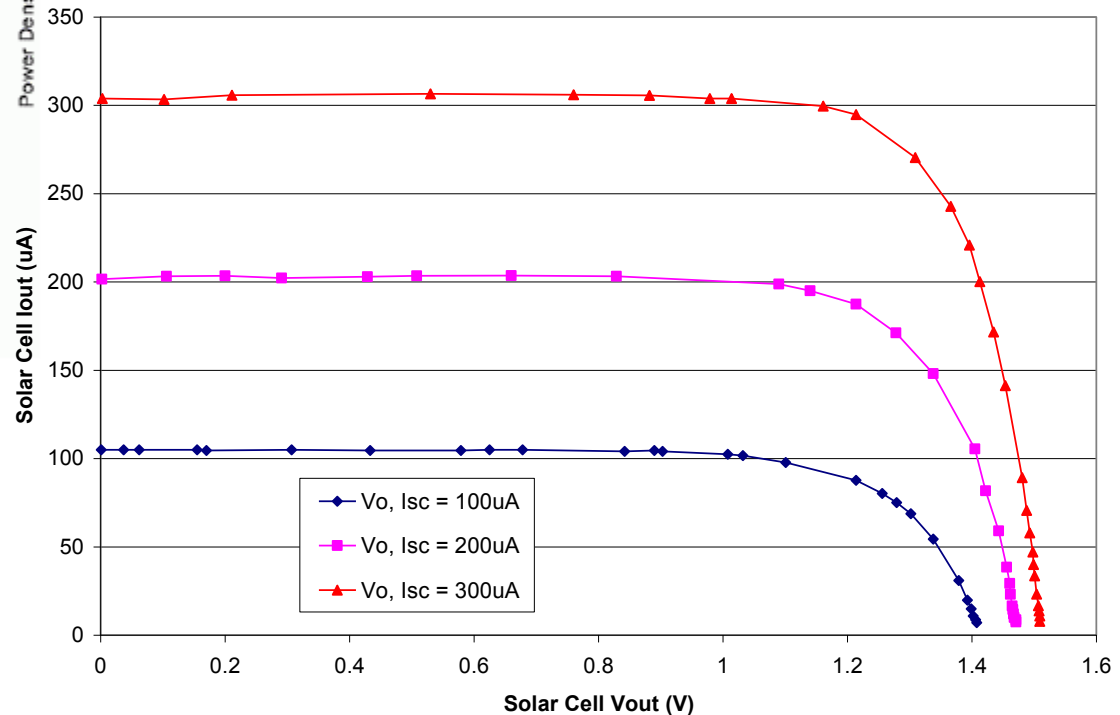
Cell Current/Voltage Behavior



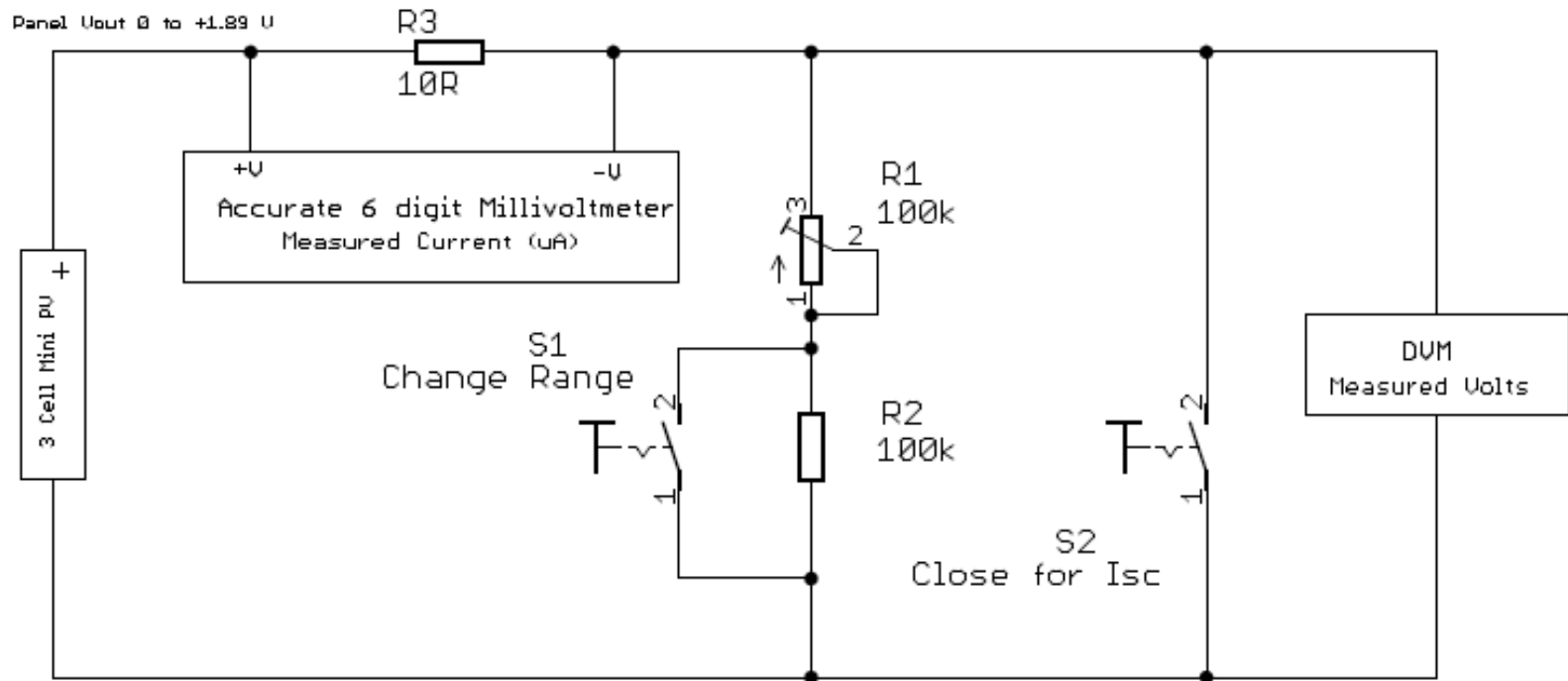
Curves provided in data sheet

Curves developed in lab in our light conditions

XOB17-04x3 IV Low Current IV Curves



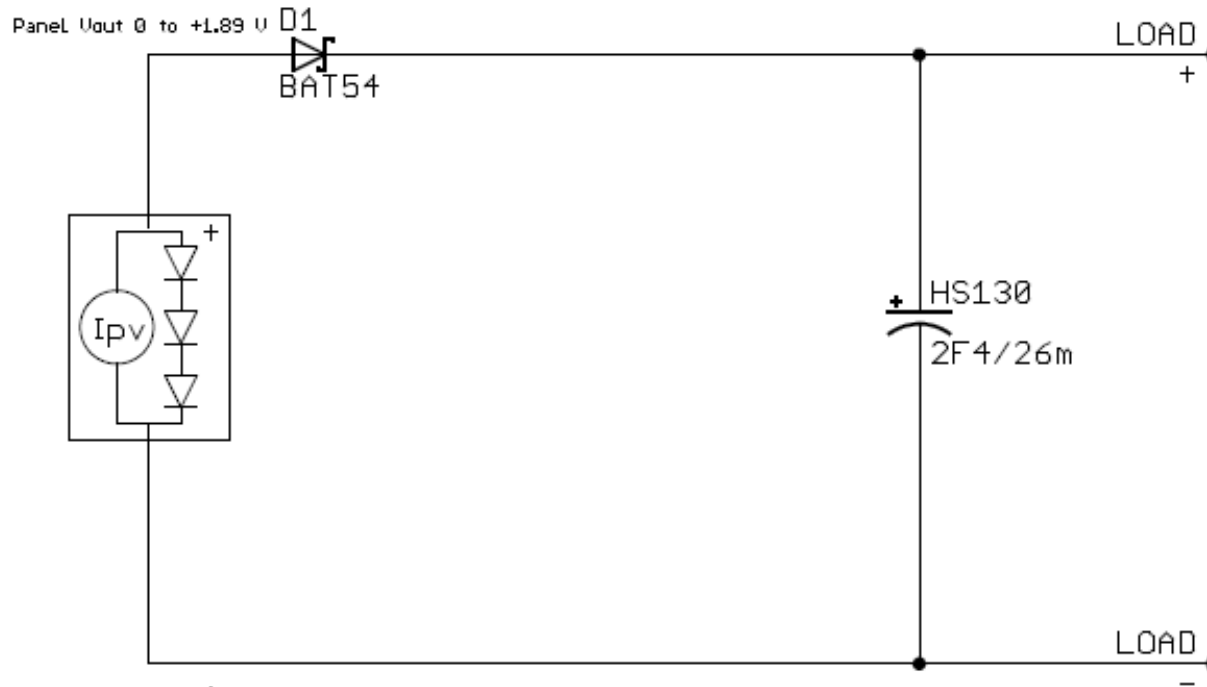
Test Circuit used to record Solar Panel IV Curves



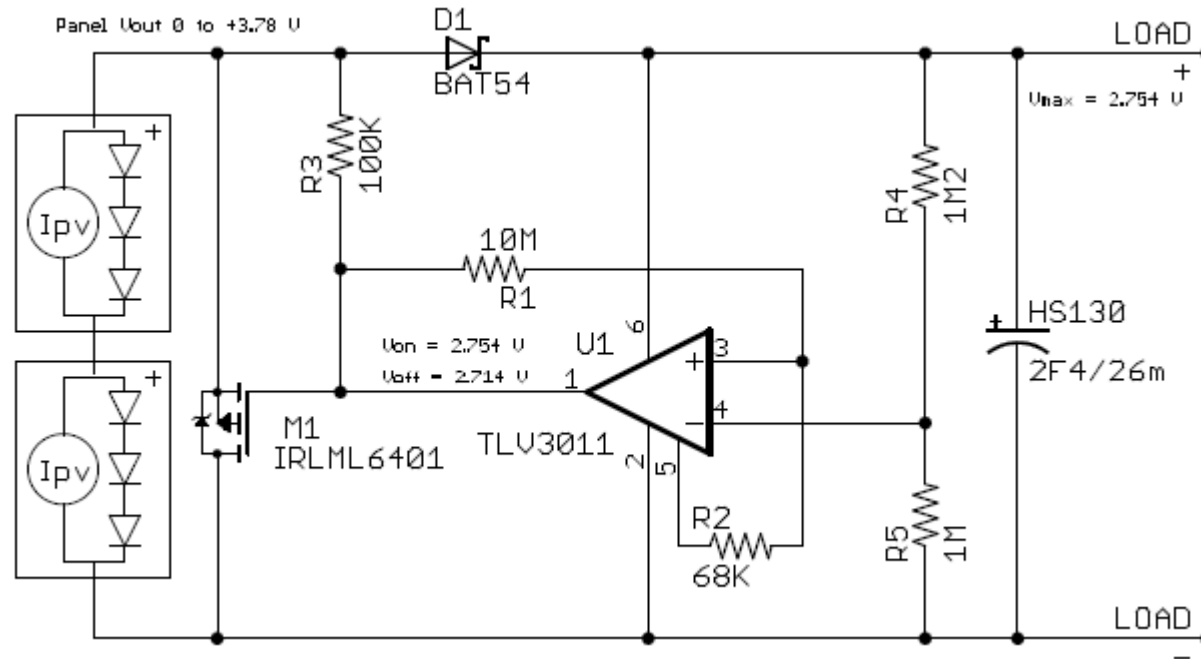
Supercapacitor Interface Circuits

Design principles:

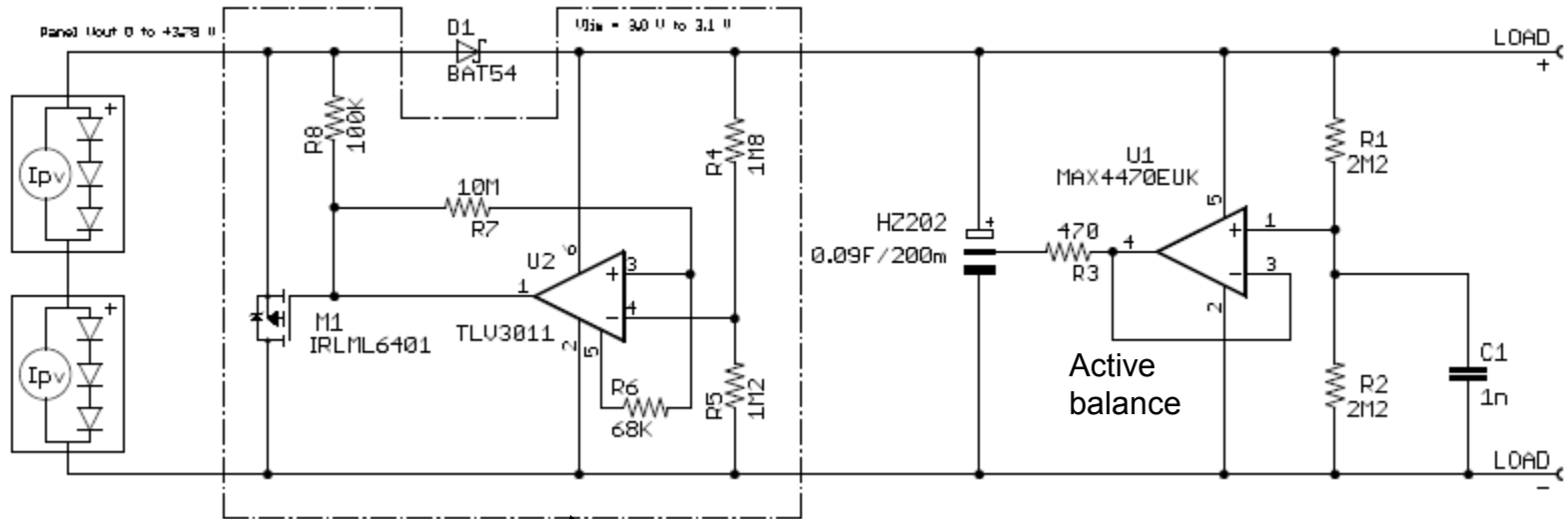
1. Must start charging from 0V
2. Must provide over voltage protection
3. Must prevent the supercapacitor from discharging into the source
4. Should be designed for maximum efficiency



- Starts charging from 0V
- $V_{oc} < 2.7V$ at max light level in the application. I-V curves of slide 25 showed $V_{oc} \approx 1.5V$
- D1 prevents supercapacitor discharging back into solar cell when light levels fall
- BAT54 chosen for D1 due to low V_F . V_F at currents $< 10\mu A$, $< 0.1V$
- HS130 provides excellent energy storage & power delivery at low voltage

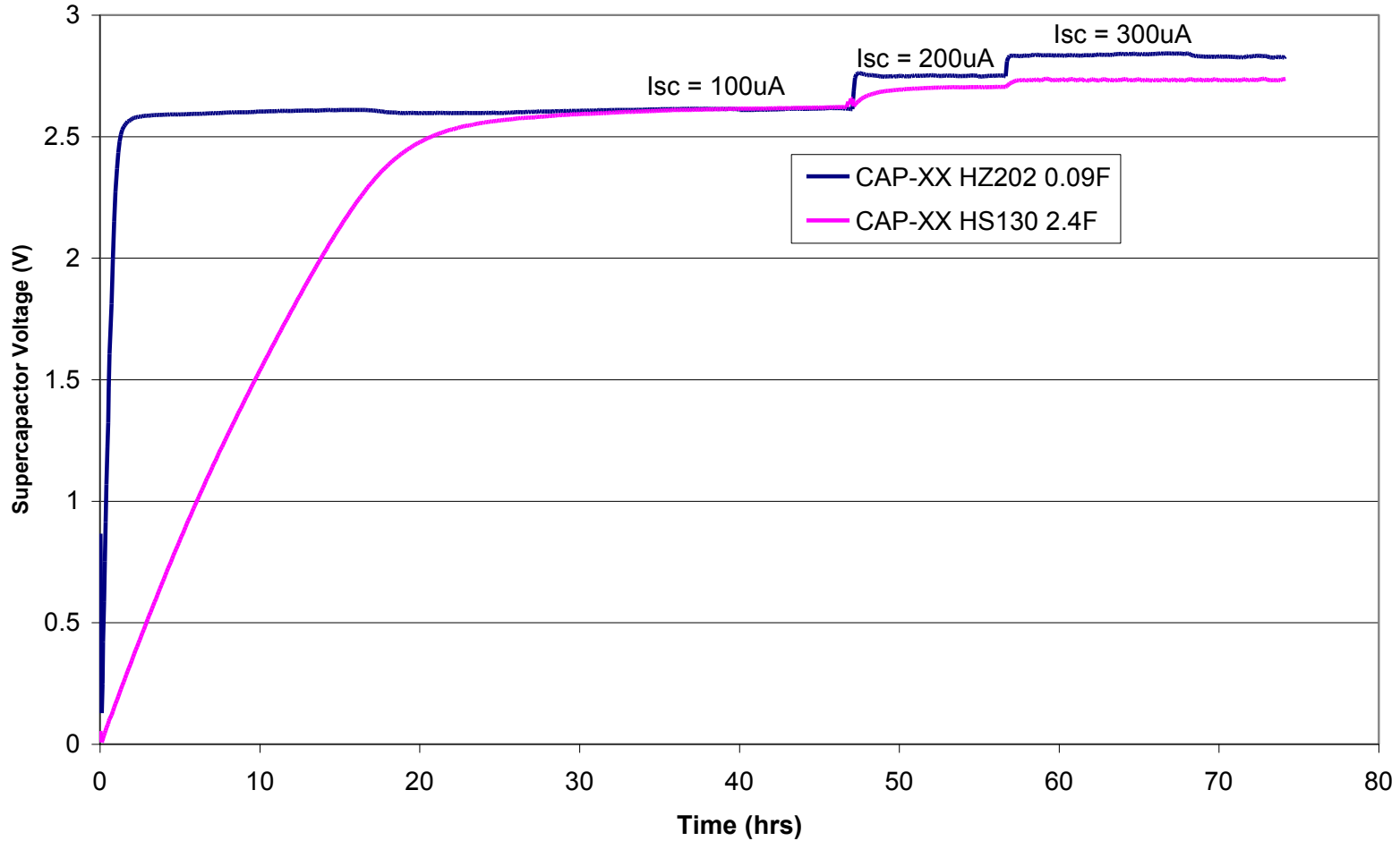


- When $V_{LOAD} > 2.75V$, turn M1 ON, VSOLAR drops & D1 does not conduct.
- When $V_{LOAD} < 2.71V$ turn M1 OFF, can charge solar cell
- TLV3011 is open drain, so o/p is open cct when $V_{scap} < 1.8V$ (min V_{ss})
- TLV3011 quiescent current $\sim 3\mu A$

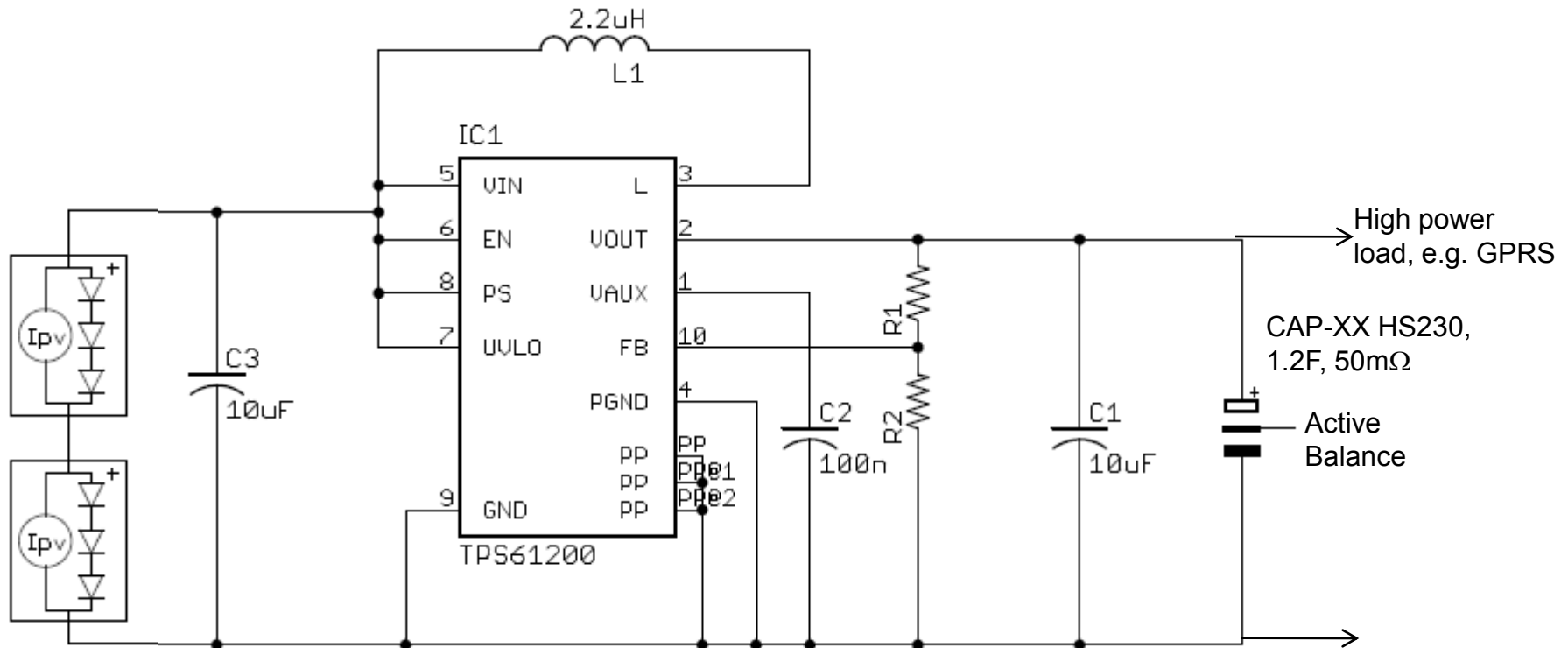


Optional over voltage control, only needed if $V_{OC} > V_{SCAP\ MAX} (= 5.5V)$

Supercapacitor Charging by Solar Bit XOB17- 04 x 3 Mini Solar Array
(Over Voltage Limiting Circuit Used)



- Previous circuits ideal for low power transmission:
 - Supercapacitor at solar cell voltage
 - with voltage regulation on load side of the supercapacitor
 - Regulator is small
- For high power, place regulator between solar cell and supercapacitor:
 - Regulator is small, low power (solar cell o/p power)
 - Supercapacitor charged to the RF PA supply voltage, supplies the RF PA directly
 - Supercapacitor must have low ESR for power delivery as well as enough energy storage to support the transmission for its duration.



- Texas Instruments TPS61200 has min $V_{in} = 300\text{mV}$, starts charging V_{aux} with load disconnected, when $V_{aux} = 2.5\text{V}$ IC starts functioning.
- Has true load disconnect (back to back PFETs as o/p switch), so supercap cannot discharge back into the source
- Uses output PFETs in linear mode to limit inrush current or limit o/p voltage if $V_{in} > V_{out}$.
- Typically draws $50\mu\text{A}$ during operation

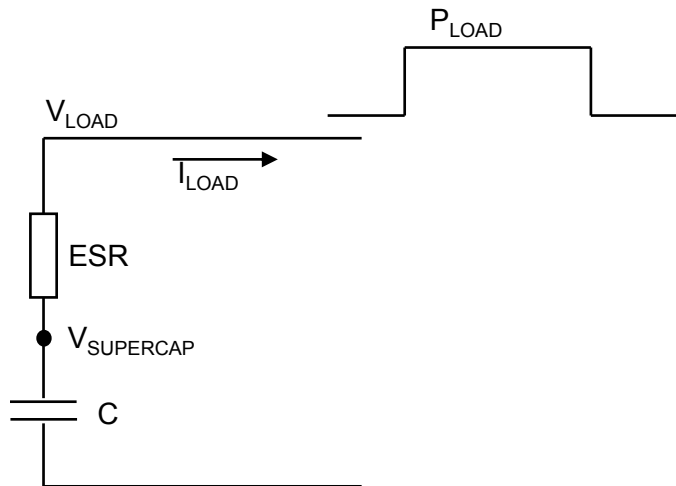
CAP-XX Single or dual cell supercapacitor?

- Single cell:
 - No balancing circuit needed
 - Lower current
 - Smaller, thinner
 - Lower cost
- Dual Cell:
 - Higher energy storage $\frac{1}{2} CV^2$
 - 5V – 1.2V, 1F → 11.8J
 - 2.5V – 1.2V, 2F → 4.8J

Energy balance approach often used: $\text{Avge Load Power} \times \text{time} = \frac{1}{2} C(V_{\text{init}}^2 - V_{\text{final}}^2)$

but

If the supercapacitor is supplying a constant power load, such as a DC:DC converter, where supercapacitor current increases as supercapacitor voltage decreases, to maintain $V \times I$ constant, then supercapacitor ESR may become significant, and you should solve:



$$V_{\text{LOAD}} = V_{\text{SUPERCAP}} - I_{\text{LOAD}} \cdot \text{ESR}$$

$$P_{\text{LOAD}} = V_{\text{LOAD}} \cdot I_{\text{LOAD}}$$

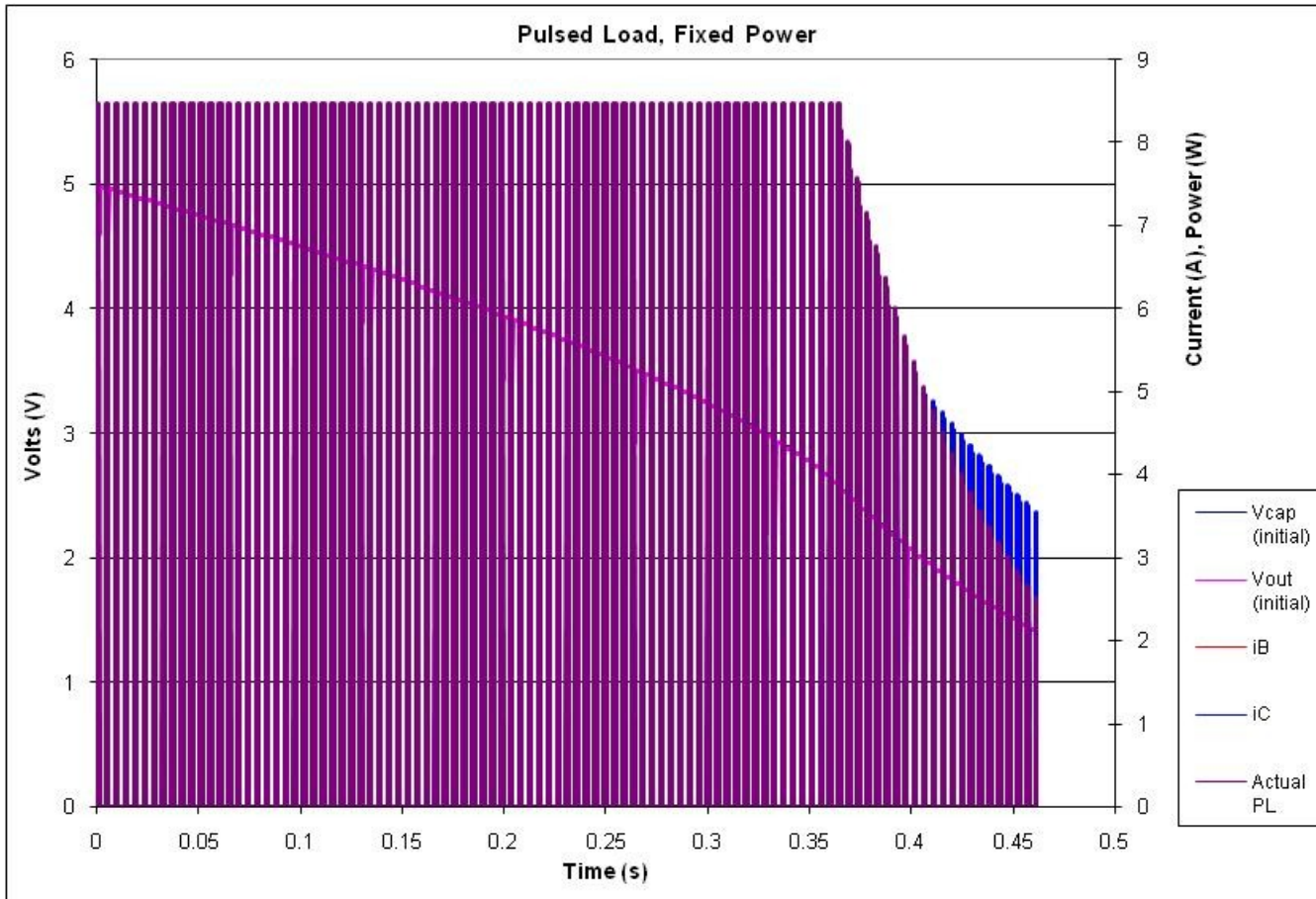
$$P_{\text{LOAD}} = (V_{\text{SUPERCAP}} - I_{\text{LOAD}} \cdot \text{ESR}) \cdot I_{\text{LOAD}}$$

$$\therefore I_{\text{LOAD}}^2 \cdot \text{ESR} - V_{\text{SUPERCAP}} \cdot I_{\text{LOAD}} + P_{\text{LOAD}} = 0$$

$$I_{\text{LOAD}} = \frac{V_{\text{SUPERCAP}} \pm \sqrt{V_{\text{SUPERCAP}}^2 - 4 \cdot \text{ESR} \cdot P}}{2 \cdot \text{ESR}}$$

If load current is very small, then $I_{\text{LOAD}} \cdot \text{ESR} \ll V_{\text{SUPERCAP}}$ and can use an energy balance to size the supercapacitor. Otherwise, use a spread sheet to solve the above and simulate V & I over time, or use SPICE.

Average load power = $25\% \times 2A \times 3.6V/85\% = 2.11W$. Load duration = $100 \text{ frames} \times 4.6ms = 0.46s$
 Load energy = $0.97J$. Supercap $V_{init} = 5V$, $V_{final} = 2.5V$
 $C = 2 \times 0.97 / (5^2 - 2.5^2) = 0.1F$. Nothing about ESR



Quadratic solution:
 $C = 0.1F$
 $ESR = 200m\Omega$

Does not work.
 $V_{final} \approx 1.5V$

Will only support
 transmission for
 0.36s

Average load power = $25\% \times 2A \times 3.6V/85\% = 2.11W$. Load duration = $100 \text{ frames} \times 4.6\text{ms} = 0.46\text{s}$
 Load energy = 0.97J . Supercap $V_{\text{init}} = 5V$, $V_{\text{final}} = 2.5V$
 $C = 2 \times 0.97 / (5^2 - 2.5^2) = 0.1F$. Nothing about ESR



Quadratic solution:

$$C = 0.13F$$

$$ESR = 200m\Omega$$

Solution works

$$V_{\text{final}} \approx 2.7V$$

- Ideal power buffer
- Low voltage, multiple cells, need cell balancing
- Leakage current decays over time, charging may take longer than expected
- Allow for ageing when selecting initial C & ESR
- Solar cells deliver max current into a short circuit – ideal for charging a supercapacitor from 0V
- Need to prevent supercapacitor discharging back into the solar cell when light falls
- Single or dual cell supercapacitor?
- Low power and high power circuits
- Remember ESR when sizing the supercapacitor

- World leader in thin, flat, small supercapacitors suitable for portable electronic devices
- Research-based, market-driven electronic components manufacturer. Founded in Australia in 1997. Listed on AIM in London, April 2006
- Turn-key power design solutions
- Production in Sydney & Malaysia
- Significant sales to big brand customers in Europe, Asia and North America
- CAP-XX supercapacitor technology licensed to Murata in 2008
- Distributors throughout USA, Europe and Asia





CAP-XX

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