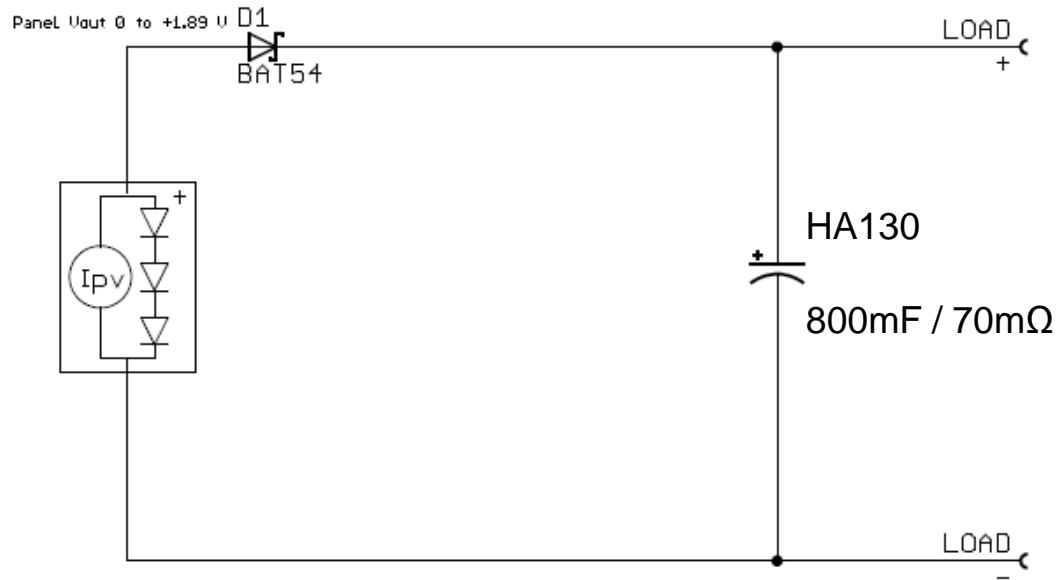

CAP-X



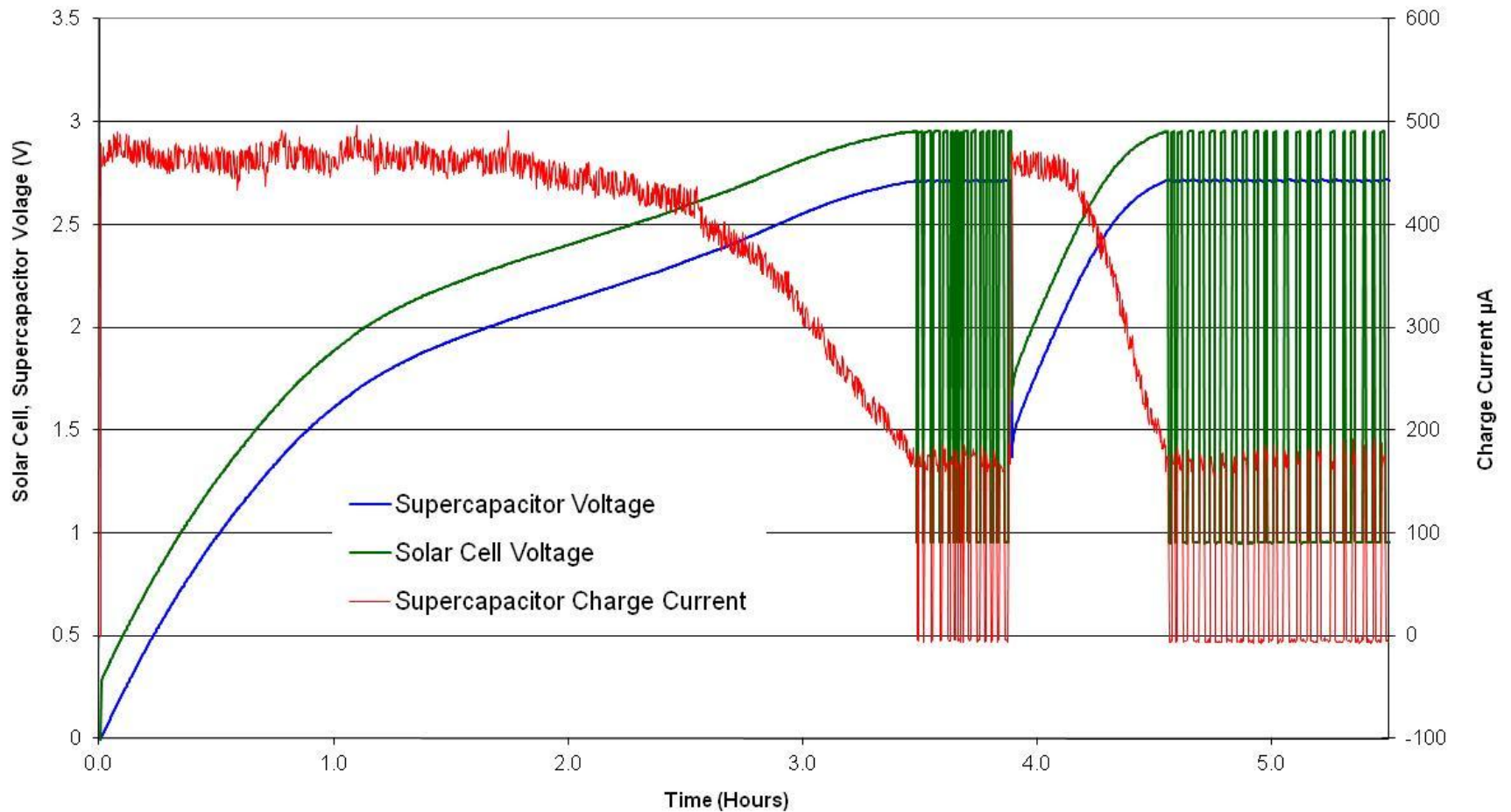
Charging a supercapacitor from a solar cell with a bq25504 PPT energy harvesting IC

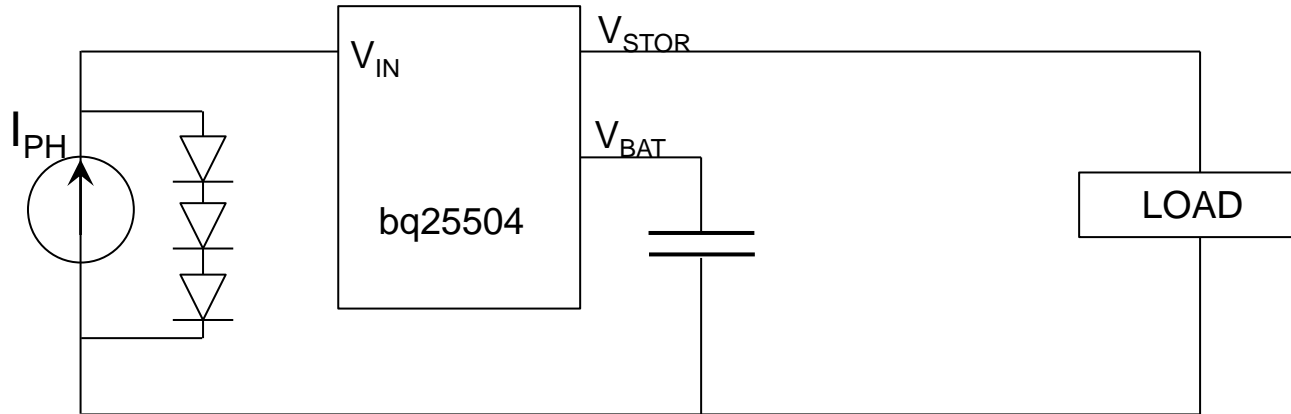
August, 2012



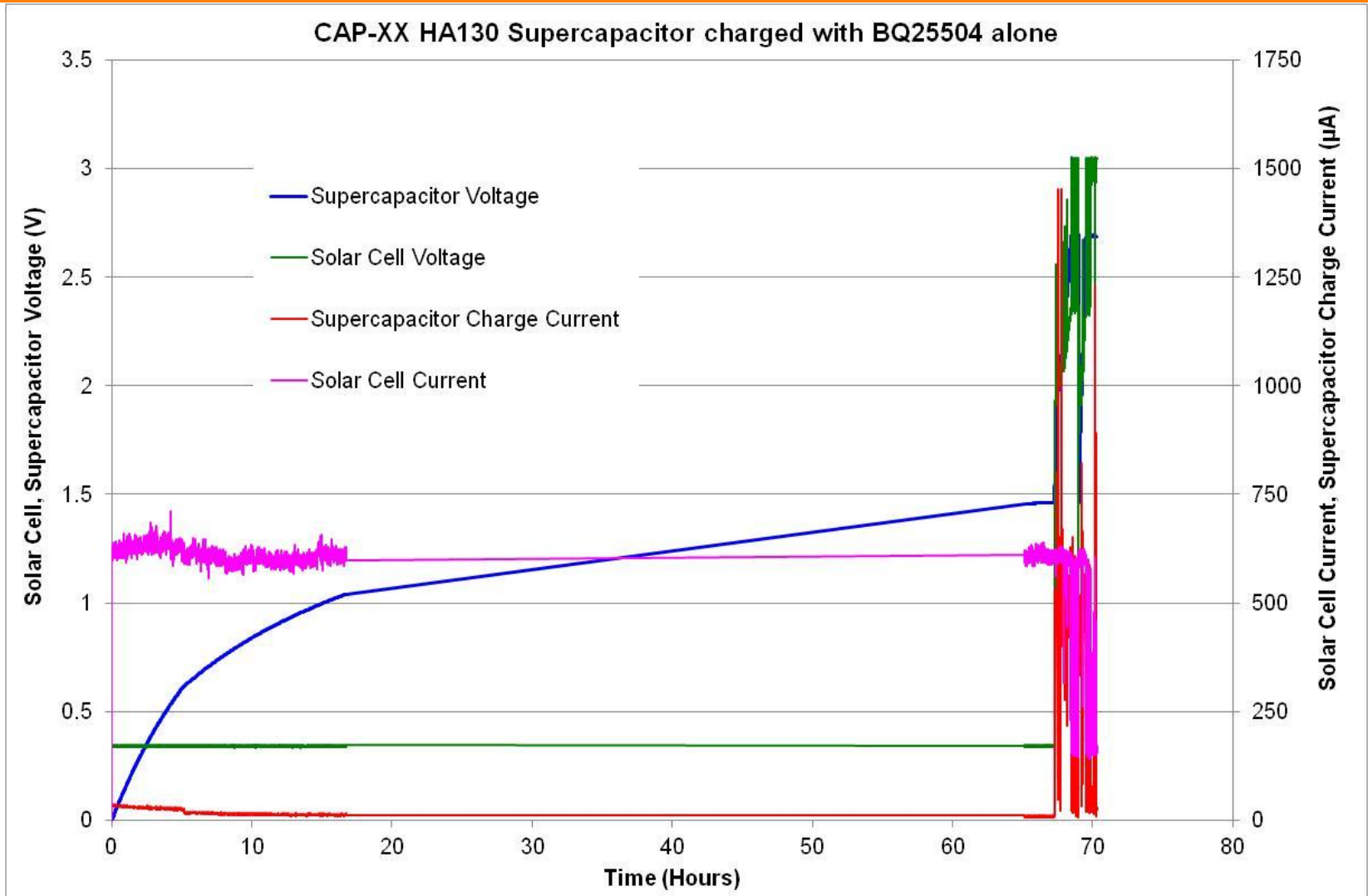
- Simplest circuit, starts charging from 0V
- $V_{OC} < 2.7V$ at maximum light level
- D1 prevents the supercapacitor from discharging back into the solar cell when light levels fall
- BAT54 chosen for D1 due to low V_F . V_F is $< 0.1V$ at currents $< 10\mu A$
- HA130 provides excellent energy storage & power delivery
- **Fastest charge. But will NOT charge if $V_{SOLAR} < V_{SCAP}$ (e.g. if light level falls)**

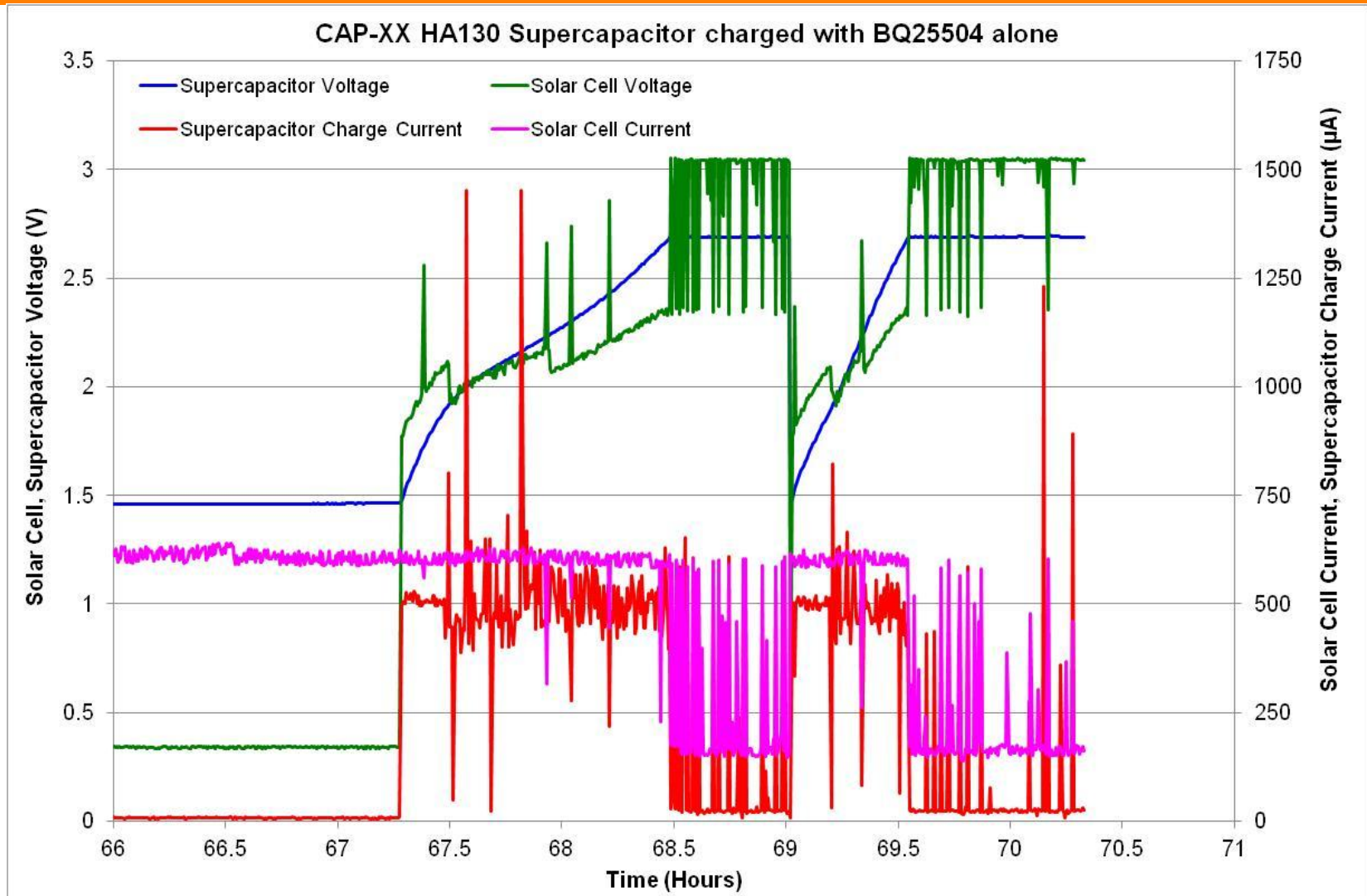
HA130 Direct Charge

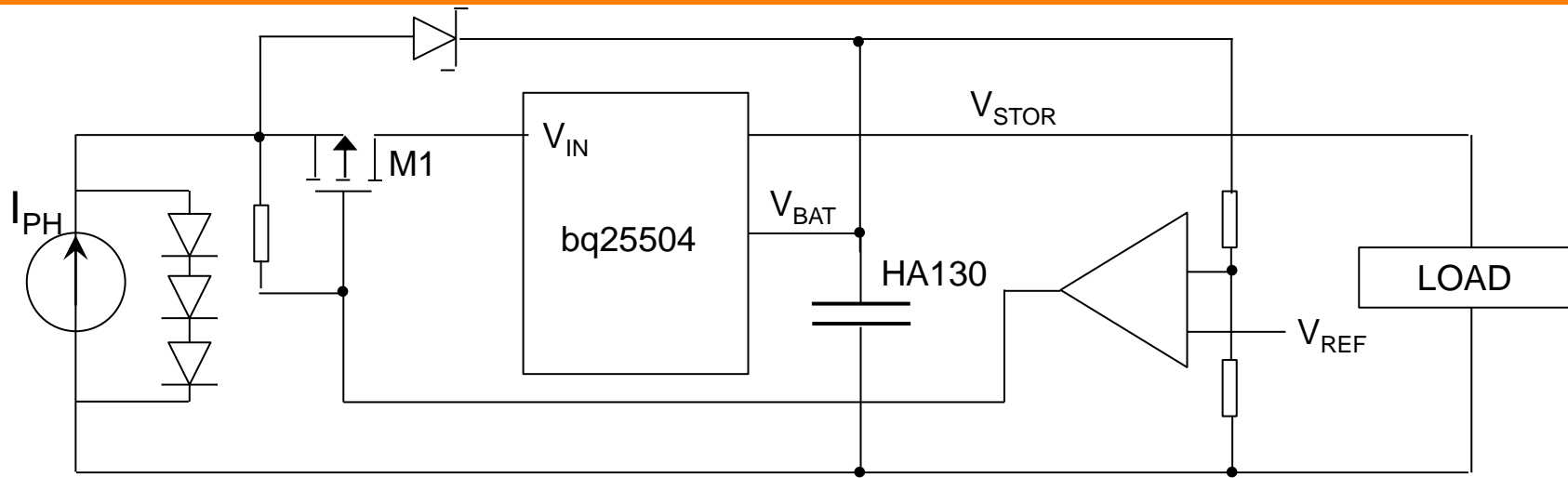




- Charge using bq25504 boost converter with Peak Power Tracking (PPT)
- The bq25504 has very inefficient “cold start” charging if $V_{BAT} < \sim 1.5V$
- It take ~ 67 hrs for the bq25504 to charge an HA130 from 0V to 1.5V with a solar cell delivering $350\mu W$ peak power (“cold start”)
- It takes another hour to reach 2.7V with the boost converter running normally with PPT
- **Slowest charge. But WILL charge if $V_{SOLAR} < V_{SCAP}$ and $V_{SCAP} > 1.5V$** (e.g. if light level falls with the supercapacitor partially or fully charged)

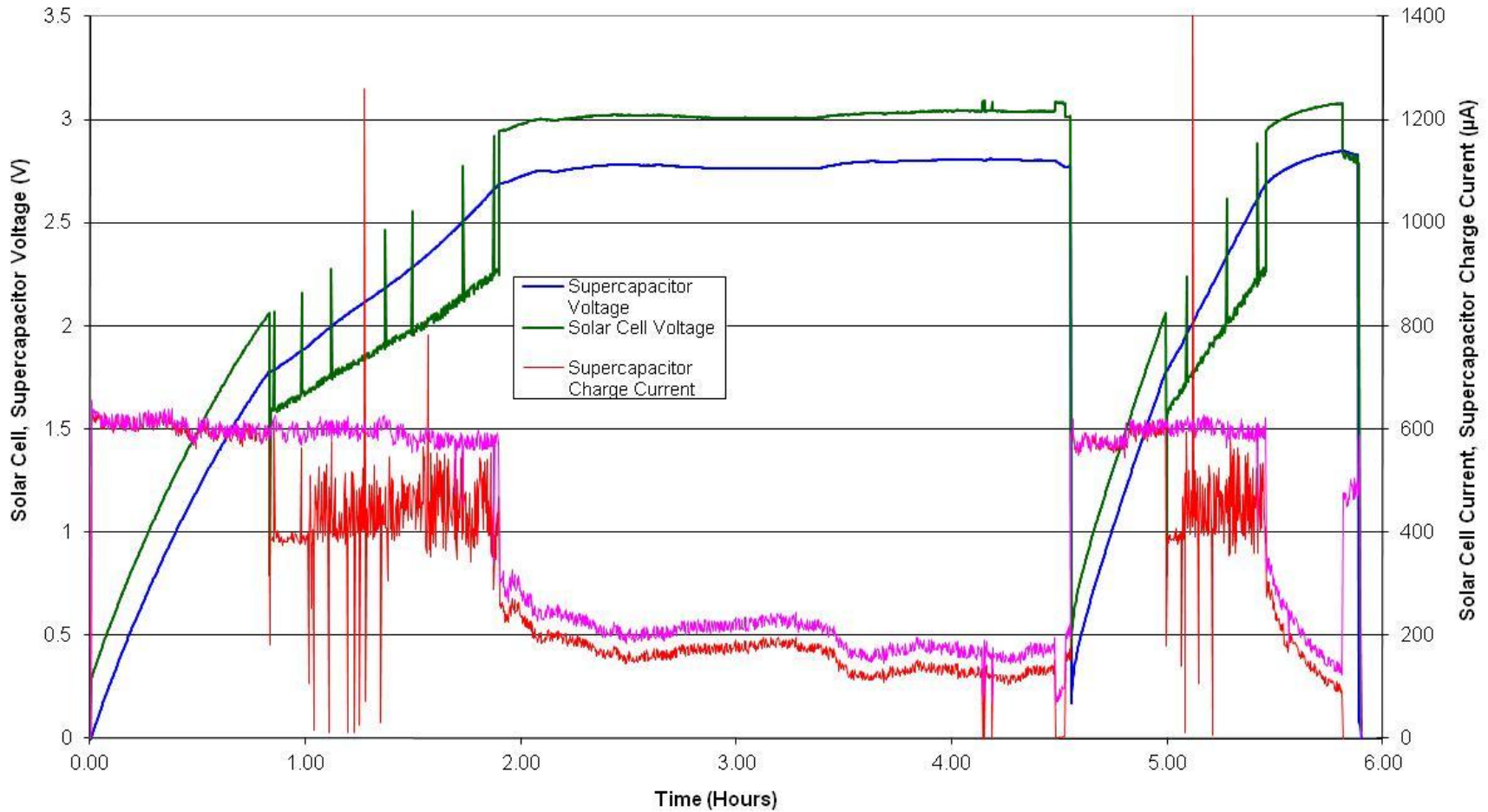


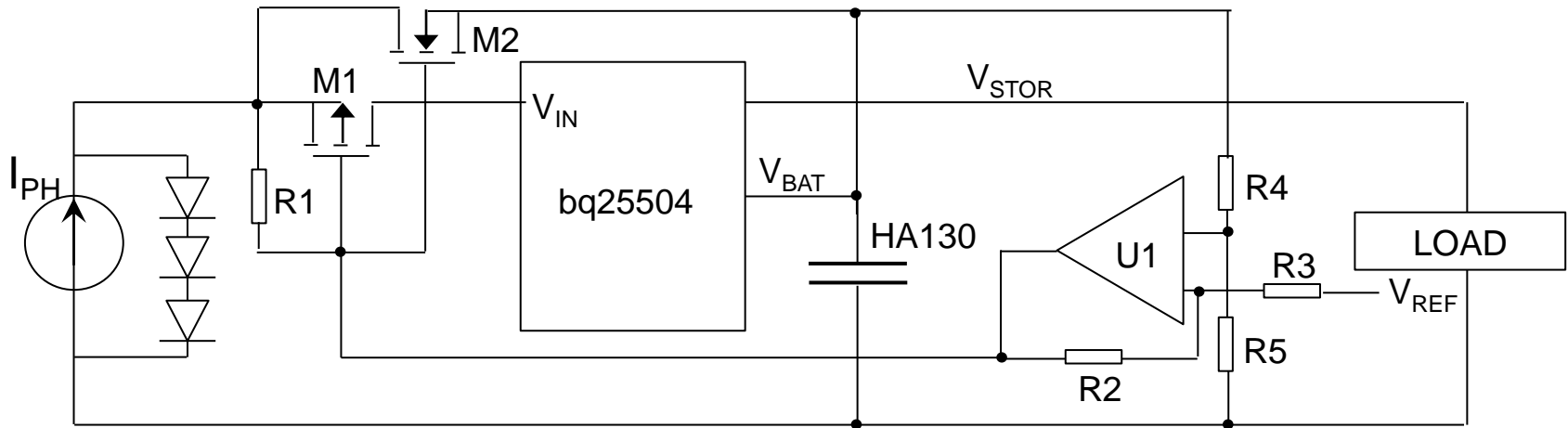




- Charge from 0V directly, using a diode to bypass the bq25504
- Much faster charging of supercapacitor to 1.5V. M1 is OFF, stopping the bq25504 from pulling down the solar cell voltage
- When the supercapacitor reaches $\sim 1.8V$, the comparator turns M1 ON, connecting the bq25504 to the solar cell
- Solar cell open circuit voltage $< 3V$ to avoid over-voltage on the supercapacitor
- Achieves fast initial charge + fast charge with PPT once $V_{SCAP} > 1.8V$
- **Fast charge, and WILL charge if $V_{SOLAR} < V_{SCAP}$ and $V_{SCAP} > 1.5V$** (e.g. if light level falls with the supercapacitor partially or fully charged)

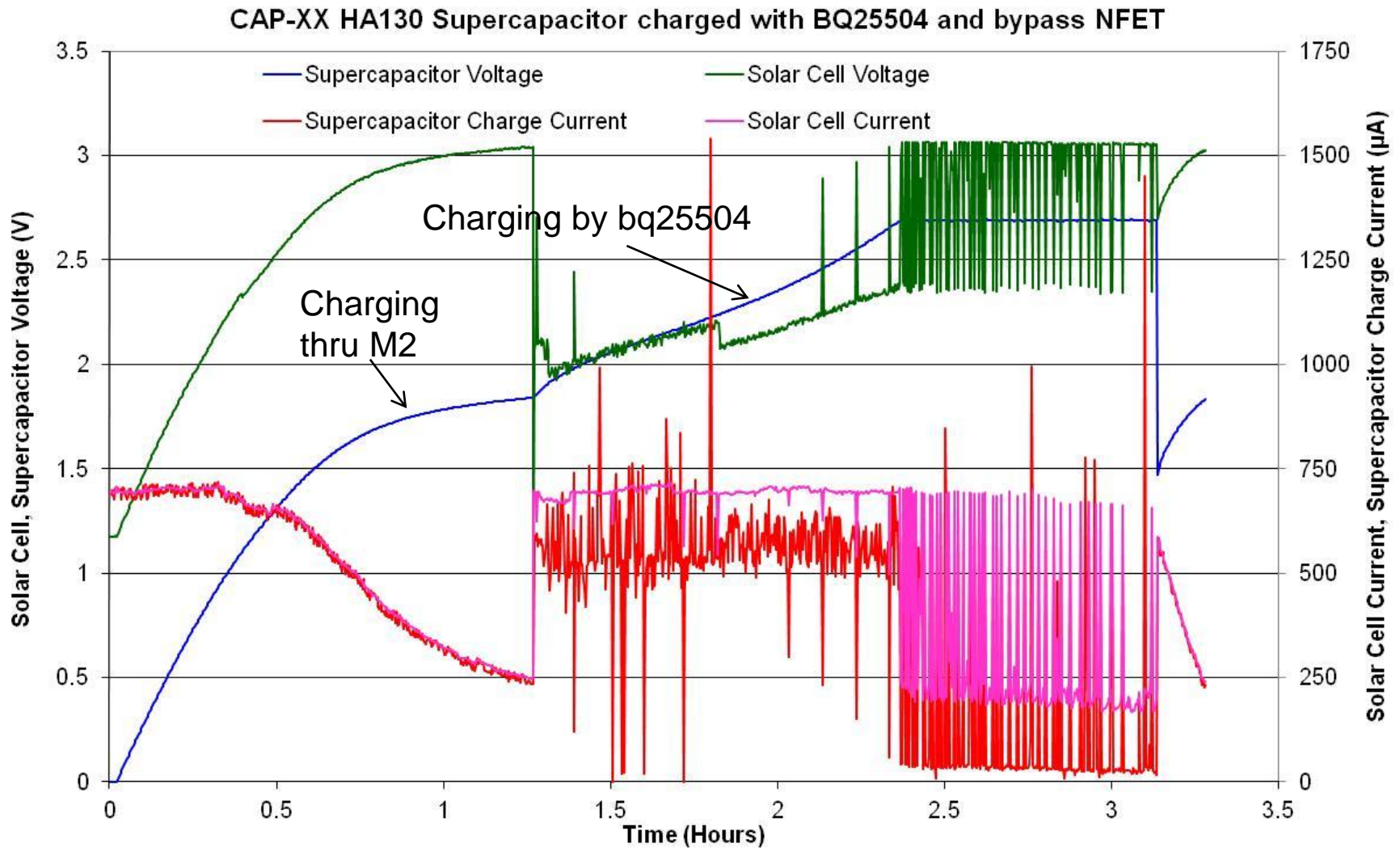
HA130 Charged with Diode then via BQ25504





- Supercap charges directly from 0V using NFET M2 to bypass bq25504. M1 is OFF, stopping the bq25504 from pulling down the solar cell voltage
- When the supercap reaches ~1.8V, the comparator turns M1 ON, connecting the bq25504 to the solar cell, and turns M2 OFF, preventing the solar cell over-charging the supercap if $V_{\text{SOLAR_OC}} > V_{\text{SCAP_MAX}}$
- The supercapacitor target voltage is now set by the bq25504. **There is no possibility of the supercapacitor being over-voltage**
- Achieve fast initial charge + fast charge with PPT once $V_{\text{SCAP}} > 1.8\text{V}$
- **Fast charge, and WILL charge if $V_{\text{SOLAR}} < V_{\text{SCAP}}$ and $V_{\text{SCAP}} > 1.8\text{V}$** (e.g. if light level falls with the supercapacitor partially or fully charged)

1. When the unit first powers ON with the supercapacitor at 0V, the source of M2 is at 0V, U1 is OFF and R1 turns M1 OFF, preventing the bq25504 from operating
2. When $V_{\text{SOLAR}} > V_{\text{GSTH}}$ of M2, M2 starts to conduct, charging the supercapacitor
3. The resistance across M2 loads the solar cell so its voltage is just above $M2(V_{\text{GSTH}}) + V_{\text{SCAP}}$ so the solar cell provides good charge current in reasonable light
4. When $V_{\text{SCAP}} = 1.85\text{V}$, the o/p of U1 goes low, turning M2 OFF, and turning M1 ON. This enables the bq25504 when the voltage at $V_{\text{BAT}} > V_{\text{STOR_CHGEN}}$, so the IC always operates in PPT mode and never in cold start mode
5. Select a low power open drain comparator with in-built reference and which operates at a supply voltage down to 1.8V or less. In our example, we used a TLV3011, which has a typical quiescent current of $2.8\mu\text{A}$ and $V_{\text{REF}} = 1.242\text{V}$. An alternative is MAX9016 with a typical quiescent current of $1\mu\text{A}$ and $V_{\text{REF}} = 1.236\text{V}$
6. Select M2 with the lowest V_{GSTH} possible, with suitable size and gate charge. The lower the V_{GSTH} , the faster the supercapacitor will reach 1.85V and enable PPT mode in the bq25504. We have used an irlm6246, which has typical V_{GSTH} of 0.8V
7. The other components used in slide 9 were: M1 = FDV302P, R1 = $1\text{M}\Omega$, R2 = $10\text{M}\Omega$, R3 = $220\text{K}\Omega$, R4 = $680\text{K}\Omega$, R5 = $1.5\text{M}\Omega$.
8. The hysteresis in the circuit means U1 will go low when $V_{\text{BAT}} > 1.85\text{V}$ and U1 will go open drain when $V_{\text{BAT}} < 1.77\text{V}$





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For more information, please contact

Pierre Mars

VP Quality & Applications Engineering

Email: pierre.mars@cap-xx.com

Web: www.cap-xx.com